

USPAS Accelerator Physics 2015 Old Dominion University

Chapter 2: Coordinates and Weak Focusing

Todd Satogata (Jefferson Lab) / <u>satogata@jlab.org</u> Vasiliy Morozov (Jefferson Lab) / <u>morozov@jlab.org</u> Alex Castilla (ODU and U. Guanajuato) / <u>acastill@jlab.org</u> <u>http://www.toddsatogata.net/2015-USPAS</u>

Happy Birthday to James Watt, Henry Bessemer, Edgar Allen Poe, Paul Cezanne, and Janis Joplin! Happy Martin Luther King Jr. Day!

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Overview

- Coordinate and reference systems
- Equations of motion in an azimuthally symmetric field
 - Elucidation of approximations
 - Transverse separability
- Solutions of equations of motion
 - 2nd order linear ODEs as matrix equations
- Momentum offsets and dispersion
- Weak focusing synchrotron
- Momentum compaction

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Connections to orbital mechanics



Parameterizing Particle Motion: Coordinates

- Now we derive more general equations of motion
- We need a local coordinate system $(\hat{x}, \hat{y}, \hat{z} \equiv \hat{s})$ relative to the design particle trajectory $\vec{B_0} = B_0 \hat{y}$ s is the direction of design particle motion y is the main magnetic field direction x is the radial direction ρ is not a coordinate, but the **design** bending radius in magnetic field B_0
- Can express total radius R as

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 $R = \rho + x \qquad \theta = \frac{s}{R} = \frac{\beta ct}{R}$

Also define local trajectory angle

$$x' \equiv \frac{dx}{ds} = \frac{1}{R} \frac{dx}{d\theta} \approx \frac{p_x}{p_0}$$



s=0

 $R = \rho + x$





Example: FNAL Coordinate Systems

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Example: CERN Coordinate Systems



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Parameterizing Particle Motion: Approximations

- We will make a few reasonable approximations:
 (A0) 0) No local currents (beam travels in a near-vacuum)
- (A1) 1) Paraxial approximation: $x', y' \ll 1$ or $p_x, p_y \ll p_0$
- (A2) 2) Perturbative coordinates: $x, y \ll \rho$
- (A3) 3) Transverse uncoupled linear magnetic field: $\vec{B} = B_0 \hat{y} + (x \hat{y} + y \hat{x}) \left(\frac{\partial B_y}{\partial x}\right)$ (A0) Note this obeys Maxwell's equations in free space (A4) 4) Negligible E field: $\gamma \approx \text{constant}$ • Equivalent to assuming adiabatically changing B fields relative to dx/dt, dy/dtefferson Lab T. Satogata / January 2015 USPAS Accelerator Physics 8

Parameterizing Particle Motion: Acceleration

Lorentz force equation of motion is

$$q\vec{v} \times \vec{B} = \frac{d(\gamma m \vec{v})}{dt} = \gamma m \dot{\vec{v}}$$
 (A4)

 Calculate velocity and acceleration in our coordinate system

$$\vec{v} = \dot{R}\hat{x} + R\dot{\hat{x}} + \dot{y}\hat{y} = \dot{R}\hat{x} + R\dot{\theta}\hat{s} + \dot{y}\hat{y}$$

$$\dot{\vec{v}} = \ddot{R}\hat{x} + (2\dot{R}\dot{\theta} + R\ddot{\theta})\hat{s} + R\dot{\theta}\dot{\hat{s}} + \ddot{y}\hat{y}$$
$$\dot{\hat{s}} = -\dot{\theta}\hat{x} = -\frac{v}{R}\hat{x}$$
So $\dot{\vec{x}} = (\ddot{D} - D\dot{\theta}\hat{z})\hat{a} + (2\dot{D}\dot{\theta}\hat{d} + D\ddot{\theta})\hat{a}$

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$$\dot{\vec{v}} = (\ddot{R} - R\dot{\theta}^2)\hat{x} + (2\dot{R}\dot{\theta} + R\ddot{\theta})\hat{s} + \ddot{y}\hat{y}$$

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 $\dot{\vec{v}} = \left| \left(\ddot{x} - \frac{v^2}{R} \right) \hat{x} \right| + \frac{2\dot{x}v}{R}\hat{s} + \frac{\ddot{y}\hat{y}}{R}\hat{s}$





Parameterizing Particle Motion: Eqn of Motion



Equations of Motion

Apply our paraxial and linearization approximations

$$p = qB_0\rho \quad R = \rho \left(1 + \frac{x}{\rho}\right)^{(A2)} B_y = B_0 + \left(\frac{\partial B_y}{\partial x}\right)^{(A3)} x \quad B_x = \left(\frac{\partial B_y}{\partial x}\right)^{(A3)} y$$
Horizontal: $\frac{d^2x}{d\theta^2} + \left(\frac{qB_y}{p}R - 1\right)R = 0$
 $\frac{d^2x}{d\theta^2} + \left[\left(1 + \frac{1}{B_0}\frac{\partial B_y}{\partial x}x\right)\left(1 + \frac{x}{\rho}\right) - 1\right]\rho\left(1 + \frac{x}{\rho}\right) = 0$
 $\Rightarrow \left[\frac{d^2x}{d\theta^2} + (1 - n)x = 0\right] \quad \text{where} \quad n \equiv -\frac{\rho}{B_0}\left(\frac{\partial B_y}{\partial x}\right)$
Vertical: $\frac{d^2y}{d\theta^2} - \frac{qB_x}{p}R^2 = 0 \quad \Rightarrow \left[\frac{d^2y}{d\theta^2} + ny = 0\right]$

Things to try sometime

- Expand the horizontal equation of motion to second order in x
 - Does it reduce to the stated equation at first order?
 - Use expansions for R, B that are still first order!
- Expand the horizontal and vertical equations of motion to second order in x, y, δ (p. 25-6 of these slides)
 - Use expansions for R, B that are still first order!

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Simple Equations of Motion!

$$\frac{d^2x}{d\theta^2} + (1-n)x = 0 \qquad \qquad \frac{d^2y}{d\theta^2} + ny = 0$$

- These are simple harmonic oscillator equations (Not surprising since we linearized 2nd order differential equations)
- These are known as the weak focusing equations
 If n does not depend on θ, stability is only possible in both
 planes if 0<n<1</p>
 This is known as the weak focusing criterion



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But Wasn't 0<n<1 Stable?

- This seems to indicate n>0 is horizontally unstable!
- Horizontal motion is a combination of two forces
 Centrifugal mv^2/R and centripetal Lorentz qvB_y Both forces cancel by definition for the design trajectory

$$F_{tot} = \frac{mv^2}{R} - qvB_y \approx \frac{mv^2}{\rho} \left(\frac{\rho}{R}\right) - qvB_0 \left(\frac{\rho}{R}\right)^n = qvB_0 \left(\frac{1}{\zeta} - \frac{1}{\zeta^n}\right)$$



where $\zeta \equiv \frac{R}{\rho}$

$$F_{tot} > 0$$
 for $\zeta < 0$
 $F_{tot} < 0$ for $\zeta > 0$

Nonlinear too! But we linearize near ζ =1





- Weak focusing formalism was originally developed for the Betatron
- Apply Faraday's law with time-varying current in coils
- Beam sees time-varying accelerating electric field too!
- Early proofs of stability: focusing and "betatron" motion

Donald Kerst UIUC 2.5 MeV Betatron, 1940

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Don' t try this at home!! T. Satogata / January 2015



UIUC 312 MeV betatron, 1949









- Separate RF cavities can eliminate the need for central iron (and corresponding huge inductance)
 - Accelerator can be (much) larger (higher energies for same B₀!)
 - But stability equation scaling with ρ is still not good:

$$0 < -\frac{\rho}{B_0} \left(\frac{\partial B_y}{\partial x}\right)_{x=0} < 1$$



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Back to Solutions of Equations of Motion

$$\frac{d^2x}{d\theta^2} + (1-n)x = 0 \qquad \qquad \frac{d^2y}{d\theta^2} + ny = 0$$

- Assume azimuthal symmetry (n does not depend on θ)
- Solutions are simple harmonic oscillator solutions

$$x(\theta) = A\cos(\theta\sqrt{1-n}) + B\sin(\theta\sqrt{1-n})$$
$$\frac{dx}{d\theta} = \sqrt{1-n}[-A\sin(\theta\sqrt{1-n}) + B\cos(\theta\sqrt{1-n})]$$

• Constants A,B are related to initial conditions (x_0, x'_0)

$$x_0 = x(\theta = 0) = A \qquad x'_0 = \frac{1}{\rho} \left(\frac{dx}{d\theta}\right)(\theta = 0) = \frac{\sqrt{1-n}}{\rho}B$$
$$A = x_0 \qquad B = \frac{\rho}{\sqrt{1-n}}x'_0$$

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Solutions of Equations of Motion

Write down solutions in terms of initial conditions

$$x(\theta) = \cos(\theta\sqrt{1-n}) x_0 + \frac{\rho}{\sqrt{1-n}} \sin(\theta\sqrt{1-n}) x'_0$$

$$x'(\theta) = \frac{1}{\rho} \frac{dx}{d\theta} = -\frac{\sqrt{1-n}}{\rho} \sin(\theta\sqrt{1-n}) x_0 + \cos(\theta\sqrt{1-n}) x'_0$$

 This can be (very) conveniently written as matrices (including both horizontal and vertical)

$$\begin{pmatrix} x(\theta) \\ x'(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{1-n}) & \frac{\rho}{\sqrt{1-n}}\sin(\theta\sqrt{1-n}) \\ -\frac{\sqrt{1-n}}{\rho}\sin(\theta\sqrt{1-n}) & \cos(\theta\sqrt{1-n}) \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$$
$$\begin{pmatrix} y(\theta) \\ y'(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{n}) & \frac{\rho}{\sqrt{n}}\sin(\theta\sqrt{n}) \\ -\frac{\sqrt{n}}{\rho}\sin(\theta\sqrt{n}) & \cos(\theta\sqrt{n}) \end{pmatrix} \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix}$$

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Transport Matrices

$$\begin{pmatrix} y(\theta) \\ y'(\theta) \end{pmatrix} = \begin{bmatrix} \cos(\theta\sqrt{n}) & \frac{\rho}{\sqrt{n}}\sin(\theta\sqrt{n}) \\ -\frac{\sqrt{n}}{\rho}\sin(\theta\sqrt{n}) & \cos(\theta\sqrt{n}) \end{bmatrix} \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix} = \begin{bmatrix} M_V(\theta) \\ y'_0 \end{pmatrix}$$

- M_V here is an example of a transport matrix
 - Linear: derived from linear equations
 - Can be concatenated to make further transformations $M_V(\theta_1+\theta_2)=M_V(\theta_1)M_V(\theta_2)$
 - Depends only on "length" θ , radius ρ , and "field" n
 - Acts to transform or transport coordinates to a new state
 - Our accelerator "lattices" will be built out of these matrices
 - Unimodular: det(M_V)=1

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- More strongly, it's symplectic: $S = M_V^T S M_V$ where $S = \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix}$
- Hamiltonian dynamics, phase space conservation (Liouville)
- These matrices here are scaled rotations!



Sinusoidal Solutions, Betatron Phases

$$\begin{pmatrix} x(\theta) \\ x'(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{1-n}) & \frac{\rho}{\sqrt{1-n}}\sin(\theta\sqrt{1-n}) \\ -\frac{\sqrt{1-n}}{\rho}\sin(\theta\sqrt{1-n}) & \cos(\theta\sqrt{1-n}) \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix} \\ \begin{pmatrix} y(\theta) \\ y'(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{n}) & \frac{\rho}{\sqrt{n}}\sin(\theta\sqrt{n}) \\ -\frac{\sqrt{n}}{\rho}\sin(\theta\sqrt{n}) & \cos(\theta\sqrt{n}) \end{pmatrix} \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix}$$

- Sinusoidal simple harmonic oscillators solutions
 - Particles move in transverse betatron oscillations around the design trajectory (x, x') = (y, y') = 0
- We define betatron phases

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$$\phi_x(s) \equiv \theta \sqrt{1-n} = \frac{s}{\rho} \sqrt{1-n} \qquad \phi_y(s) \equiv \theta \sqrt{n} = \frac{s}{\rho} \sqrt{n}$$

Write matrix equation in terms of s rather than $\boldsymbol{\theta}$

$$\begin{pmatrix} x(s) \\ x'(s) \end{pmatrix} = \begin{pmatrix} \cos \phi_x(s) & \frac{\rho}{\sqrt{1-n}} \sin \phi_x(s) \\ -\frac{\sqrt{1-n}}{\rho} \sin \phi_x(s) & \cos \phi_x(s) \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$$



Visualization of Betatron Oscillations

Simplest case: constant uniform vertical field (n=0)



More complicated strong focusing



with tune: $Q_h = 6.3$, i.e., 6.3 oscillations per turn.

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theta

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sine-like

Vertical Betatron Oscillation with tune: Q_v = 7.5, i.e., 7.5 oscillations per turn.

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design

Visualization of Betatron Oscillations, Tunes

- What happens for 0<n<1?</p>
 - Example picture below has 5 "turns" with $sin(0.89 \theta)$
 - The betatron oscillation precesses, not strictly periodic
 - Betatron tune Q_{X,Y}: number of cycles made for every revolution or turn around accelerator

$$Q_x = \frac{1}{2\pi}\sqrt{1-n}(2\pi) = \sqrt{1-n}$$

$$Q_y = \frac{1}{2\pi}\sqrt{n}(2\pi) = \sqrt{n}$$
Frequency of betatron oscillations relative to turns around accelerator
$$Q_x^2 + Q_y^2 = 1$$
For weak focusing:
$$Q_x^2 + Q_y^2 = 1$$
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Transport Matrices: Piecewise Solutions

$$\begin{pmatrix} y(\theta) \\ y'(\theta) \end{pmatrix} = \begin{bmatrix} \cos(\theta\sqrt{n}) & \frac{\rho}{\sqrt{n}}\sin(\theta\sqrt{n}) \\ -\frac{\sqrt{n}}{\rho}\sin(\theta\sqrt{n}) & \cos(\theta\sqrt{n}) \end{bmatrix} \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix} = \boxed{M_V(\theta)} \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix}$$

 Linear transport matrices make piecewise solutions of equations of motion accessible



Transport Matrices: Accelerator Legos

With linear fields, there are two basic types of Legos

- Dipoles $\vec{B} = B_0 \hat{y} + (x \hat{y} + y \hat{x}) \left(\frac{\partial B_y}{\partial x}\right)$ $B_0 \neq 0$
 - Often long magnets to bend design trajectory
 - Entrance/exit locations can become important
 - May or may not include focusing ("combined function")
 - Special case: drift when all B components are zero

• Quadrupoles
$$\vec{B} = (x\hat{y} + y\hat{x})\left(\frac{\partial B_y}{\partial x}\right)$$
 $B_0 = 0$

- Design trajectory is straight! (no fields at x=y=0)
- Act to focus particles moving off of design trajectory
- Special case: "thin lens" approximation
- We'll talk about quadrupoles tomorrow

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Transport Matrices: Dipole

 We have already derived a very general transport matrix for a dipole magnet with focusing

$$\begin{pmatrix} x(s)\\ x'(s)\\ y(s)\\ y'(s) \end{pmatrix} = \begin{pmatrix} \cos\phi_x(s) & \frac{\rho}{\sqrt{1-n}}\sin\phi_x(s) & 0 & 0\\ -\frac{\sqrt{1-n}}{\rho}\sin\phi_x(s) & \cos\phi_x(s) & 0 & 0\\ 0 & 0 & \cos\phi_y(s) & \frac{\rho}{\sqrt{n}}\sin\phi_y(s)\\ 0 & 0 & -\frac{\sqrt{n}}{\rho}\sin\phi_y(s) & \cos\phi_y(s) \end{pmatrix} \begin{pmatrix} x_0\\ x'_0\\ y_0\\ y'_0 \end{pmatrix}$$
$$\phi_x(s) \equiv \theta\sqrt{1-n} = \frac{s}{\rho}\sqrt{1-n} \quad \phi_y(s) \equiv \theta\sqrt{n} = \frac{s}{\rho}\sqrt{n}$$

 Taking n->0 (and being careful) gives the transport matrix for a dipole of bend angle θ without focusing

$$\begin{pmatrix} x(s) \\ x'(s) \\ y(s) \\ y'(s) \end{pmatrix} = \begin{pmatrix} \cos\theta & \rho\sin\theta & 0 & 0 \\ -\frac{1}{\rho}\sin\theta & \cos\theta & 0 & 0 \\ 0 & 0 & 1 & \rho\theta \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \\ y_0 \\ y'_0 \end{pmatrix}$$

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$\begin{pmatrix} x(s) \\ x'(s) \\ y(s) \\ y'(s) \end{pmatrix} = \begin{pmatrix} \cos\theta & \rho\sin\theta & 0 & 0 \\ -\frac{1}{\rho}\sin\theta & \cos\theta & 0 & 0 \\ 0 & 0 & 1 & \rho\theta \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \\ y_0 \\ y'_0 \end{pmatrix}$

- For n=0, there is no horizontal field or vertical force
 - The vertical transport matrix here is for a field-free drift
 - This applies in both x,y planes when there is no field





Weak Focusing Synchrotron Parameterization

 We can write the cell transport matrix M_H in a form that is very similar to a rotation matrix

$$M_H = \begin{pmatrix} \cos \mu_H & \beta_H \sin \mu_H \\ -\frac{1}{\beta_H} \sin \mu_H & \cos \mu_H \end{pmatrix}$$

- We will investigate this parameterization (and its nonperiodic lattice extensions) extensively later this week
- β_H is a length scale for the betatron oscillations
- Details in Section 2.5 derive:

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$$\beta_H \approx \frac{\rho}{\sqrt{1-n}} \left(1 + \frac{l_0}{\pi \rho} \right) \qquad \beta_V \approx \frac{\rho}{\sqrt{n}} \left(1 + \frac{l_0}{\pi \rho} \right)$$

• Note the familiar scaling with the radius of curvature ρ !



What About Momentum?

- So far we have assumed that the design trajectory particle and our particle have the same momentum
- How do equations change if we break this assumption?
 - Expect only horizontal motion changes to first order (A2)

$$p = p_0(1+\delta) \text{ where } \delta \equiv \frac{\Delta p}{p_0} \ll 1 \qquad p_0 = \text{design particle momentum}$$

$$\frac{d^2 x}{d\theta^2} + \left(\frac{qB_y}{p}R - 1\right)R = 0 \implies \frac{d^2 x}{d\theta^2} + \left(\frac{qB_y}{p_0(1+\delta)}R - 1\right)R = 0$$

$$\frac{d^2 x}{d\theta^2} + \left(\frac{qB_y}{p_0}(1-\delta)R - 1\right)R = 0$$

$$\frac{d^2 x}{d\theta^2} + \left(\frac{qB_y}{p_0}R - 1\right)R = \delta \frac{R^2 qB_y}{p_0} = \rho \delta$$

$$\frac{d^2 x}{d\theta^2} + (1-n)x = \rho \delta$$
Add inhomogeneous term to original $\delta = 0$ equation of motion
Example 1

$$Add = 0$$

$$Add = 0$$

$$Add = 0$$

$$Add = 0$$



Solutions of Dispersive Equations of Motion

$$\frac{d^2x}{d\theta^2} + (1-n)x = \rho\delta \qquad \qquad \frac{d^2y}{d\theta^2}$$

- This momentum effect is called dispersion
 - Similar to prism light dispersion in classical optics
- Solutions are simple harmonic oscillator solutions
 - But now we add a specific inhomogeneous solution

$$x(\theta) = A\cos(\theta\sqrt{1-n}) + B\sin(\theta\sqrt{1-n}) + \frac{\rho}{1-n}\delta$$
$$\frac{dx}{d\theta} = \sqrt{1-n}[-A\sin(\theta\sqrt{1-n}) + B\cos(\theta\sqrt{1-n})]$$

Constants A,B again related to initial conditions (x_0, x'_0)

$$A = x_0 - \frac{\rho}{1-n}\delta \qquad B = \frac{\rho}{\sqrt{1-n}}x'_0$$

 δ is constant (A4)

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+ny=0





inhomogeneous term!

Solutions of Dispersive Equations of Motion

Write down solutions in terms of initial conditions

$$x'(\theta) = -\frac{\sqrt{1-n}}{\rho}\sin(\theta\sqrt{1-n})x_0 + \cos(\theta\sqrt{1-n})x'_0 + \frac{1}{\sqrt{1-n}}\sin(\theta\sqrt{1-n})\delta_0$$
$$x'(\theta) = \frac{1}{\rho}\frac{dx}{d\theta} = -\frac{\sqrt{1-n}}{\rho}\sin(\theta\sqrt{1-n})x_0 + \cos(\theta\sqrt{1-n})x'_0 + \frac{1}{\sqrt{1-n}}\sin(\theta\sqrt{1-n})\delta_0$$
$$\delta = \delta_0$$

 This can be now be "conveniently" written in terms of a 3x3 matrix:

$$\begin{pmatrix} x(\theta) \\ x'(\theta) \\ \delta(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{1-n}) & \frac{\rho}{\sqrt{1-n}}\sin(\theta\sqrt{1-n}) & \frac{\rho}{1-n}[1-\cos(\theta\sqrt{1-n})] \\ -\frac{\sqrt{1-n}}{\rho}\sin(\theta\sqrt{1-n}) & \cos(\theta\sqrt{1-n}) & \frac{1}{\sqrt{1-n}}\sin(\theta\sqrt{1-n}) \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \\ \delta_0 \end{pmatrix}$$

As usual, this can be simplified for n=0 (pure dipole) Note that δ has become a "coordinate"!

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Sector Dipole Magnets

- This transport matrix applies for **any** angle θ
- So it is also the transport matrix of any section of constant field, and now includes dispersion.
 - In particular, it is the horizontal transport for a combined function sector dipole of length $L = \rho \theta$
 - With n=0 this is the horizontal transport for a **sector dipole** of length $L = \rho \theta$, bend angle θ , and radius of curvature ρ

$$\mathbf{M}_{\text{dipole}} = \begin{pmatrix} \cos\theta & \rho\sin\theta & \rho(1-\cos\theta) \\ -\frac{1}{\rho}\sin\theta & \cos\theta & \sin\theta \\ 0 & 0 & 1 \end{pmatrix}$$

 Sector dipole: design trajectory at entrance and exit of magnet is perpendicular to magnet face

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Example: 180 Degree Dipole Magnet

$$\begin{pmatrix} x(\theta)\\ x'(\theta)\\ \delta(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{1-n}) & \frac{\rho}{\sqrt{1-n}}\sin(\theta\sqrt{1-n}) & \frac{\rho}{1-n}[1-\cos(\theta\sqrt{1-n})] \\ -\frac{\sqrt{1-n}}{\rho}\sin(\theta\sqrt{1-n}) & \frac{1}{\sqrt{1-n}}\sin(\theta\sqrt{1-n}) \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_0\\ x'_0\\ \delta_0 \end{pmatrix}$$

$$n = 0 \Rightarrow M_H(\theta) = \begin{pmatrix} \cos\theta & \rho\sin\theta & \rho(1-\cos\theta) \\ -\frac{1}{\rho}\sin\theta & \cos\theta & \sin\theta \\ 0 & 0 & 1 \end{pmatrix}$$

$$n = 0, \ \theta = \pi \Rightarrow M_H(\theta) = \begin{pmatrix} -1 & 0 & 2\rho \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$ror initial coordinates \begin{pmatrix} 0\\ 0\\ \pm\delta \end{pmatrix} \qquad electrons moving through uniform vertical B field \\ \otimes & \otimes & \otimes \\ \begin{pmatrix} x\\ x'\\ \delta \end{pmatrix} = \begin{pmatrix} -1 & 0 & 2\rho \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 0\\ 0\\ \pm\delta \end{pmatrix} = \begin{pmatrix} \pm 2\rho\delta \\ 0\\ \pm\delta \end{pmatrix} \qquad \bigotimes & \bigotimes \\ P \qquad 2(\rho-d\rho) - \rho \qquad 2(\rho+d\rho)$$

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Momentum Compaction

- Different momenta particles will have different path lengths $L \equiv \oint ds$ around the accelerator
 - Naively larger $p \to \text{larger } \rho \to \text{larger } L$
 - This is not necessarily true (as we'll see!)
- This is quantified by a quantity called momentum compaction
 - Ratio of fractional change in pathlength to fractional change in momentum

$$\alpha_p \equiv \frac{(dL/L)}{(dp/p)} = \frac{p}{L} \frac{dL}{dp}$$



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Transition Energy

- Relativistic particle motion in a periodic accelerator (like a synchrotron) creates some weird effects
 - For particles moving around with frequency ω in circumference C

$$\omega = \frac{2\pi\beta c}{C} \quad \Rightarrow \quad \frac{d\omega}{\omega} = \frac{d\beta}{\beta} - \frac{dC}{C} = \left(\frac{1}{\gamma^2} - \frac{1}{\gamma_{tr}^2}\right)\delta$$

momentum compaction $\alpha_p \equiv \frac{dC}{C}/\delta = \frac{p}{C}\frac{dC}{dp}$ transition gamma $\gamma_{tr} \equiv \frac{1}{\sqrt{\alpha_p}}$
• At "transition", $\gamma = \gamma_{tr}$ and particle revolution frequency does not
depend on its momentum
Reminiscent of a cyclotron but now we're strong focusing and at constant
radius!
electron ring
electron linac At $\gamma_r > \gamma_{tr}$ higher momentum gives lower revolution frequency
At $\gamma_r < \gamma_{tr}$ higher momentum gives higher revolution frequency
Hadron synchrotrons can accelerate through transition!
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Momentum Compaction: A Classic Example

- Consider a satellite in circular orbit
- A classical gravity/centripetal force problem

$$F = \frac{GMm}{R^2} = \frac{mv^2}{R}$$

$$\frac{GM}{R} = v^2 \qquad \omega = 2\pi f = 2\pi \left(\frac{v}{2\pi R}\right) = \frac{v}{R}$$
momentum compaction $\alpha_p \equiv \frac{dC}{C} / \frac{dp}{p} = \frac{dR}{R} / \frac{dv}{v} = \frac{v}{R} / \frac{dv}{dR}$

$$2v \ dv = -\frac{GM}{R^2} dR \quad \Rightarrow \quad \frac{dv}{dR} = -\frac{v}{2R}$$

$$\boxed{\text{momentum compaction } \alpha_p = -2}$$
Raising momentum p lowers orbit radius, raises angular frequency ω
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