

USPAS Accelerator Physics 2017

University of California, Davis

Chapter 2: Coordinates and Weak Focusing

Todd Satogata (Jefferson Lab and ODU) / satogata@jlab.org

Cedric Hernalsteens (IBA) / cedric.hernalsteens@gmail.com

Randika Gamage (ODU) / bgama002@odu.edu

<http://www.toddsatogata.net/2017-USPAS>

Happy Birthday to Jill Sobule, Susan Sontag, Jill Tarter, and Robert L. Park!
Happy Martin Luther King Jr. Day and Appreciate a Dragon Day!

Overview

- Coordinate and reference systems
- Equations of motion in an azimuthally symmetric field
 - e.g. betatron a particular point in time
 - Elucidation of approximations
 - Transverse separability
- Solutions of equations of motion
 - 2nd order linear ODEs as matrix equations
- Momentum offsets and dispersion
- Weak focusing synchrotron
- Momentum compaction
 - Connections to orbital mechanics

2.1: Parameterizing Particle Motion: Coordinates

- Now we derive more general equations of motion
- We need a **local coordinate system** $(\hat{x}, \hat{y}, \hat{z} \equiv \hat{s})$
relative to the design particle trajectory

s is the direction of design particle motion

y is the main magnetic field direction

x is the radial direction

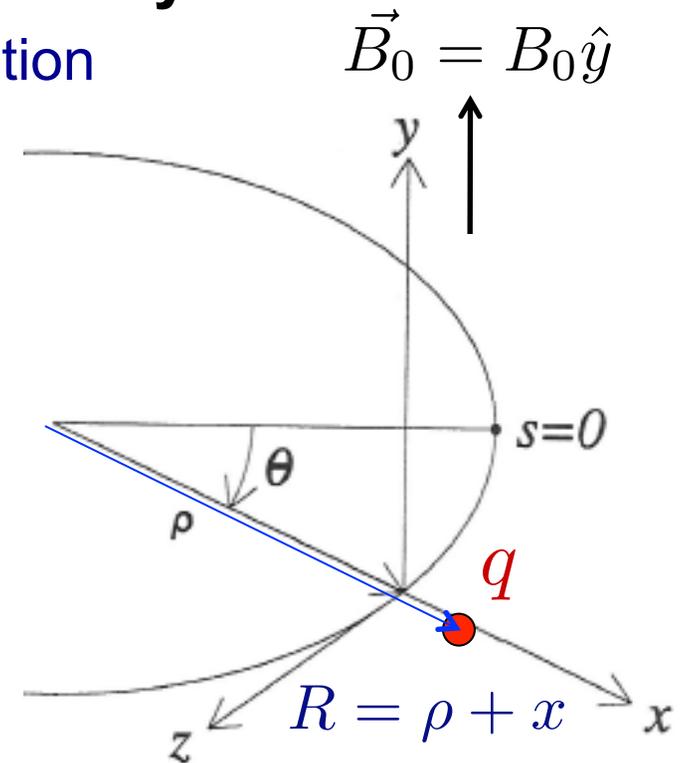
ρ is not a coordinate, but the **design**
 bending radius in magnetic field B_0

- Can express total radius R as

$$R = \rho + x \quad \theta = \frac{s}{R} = \frac{\beta ct}{R}$$

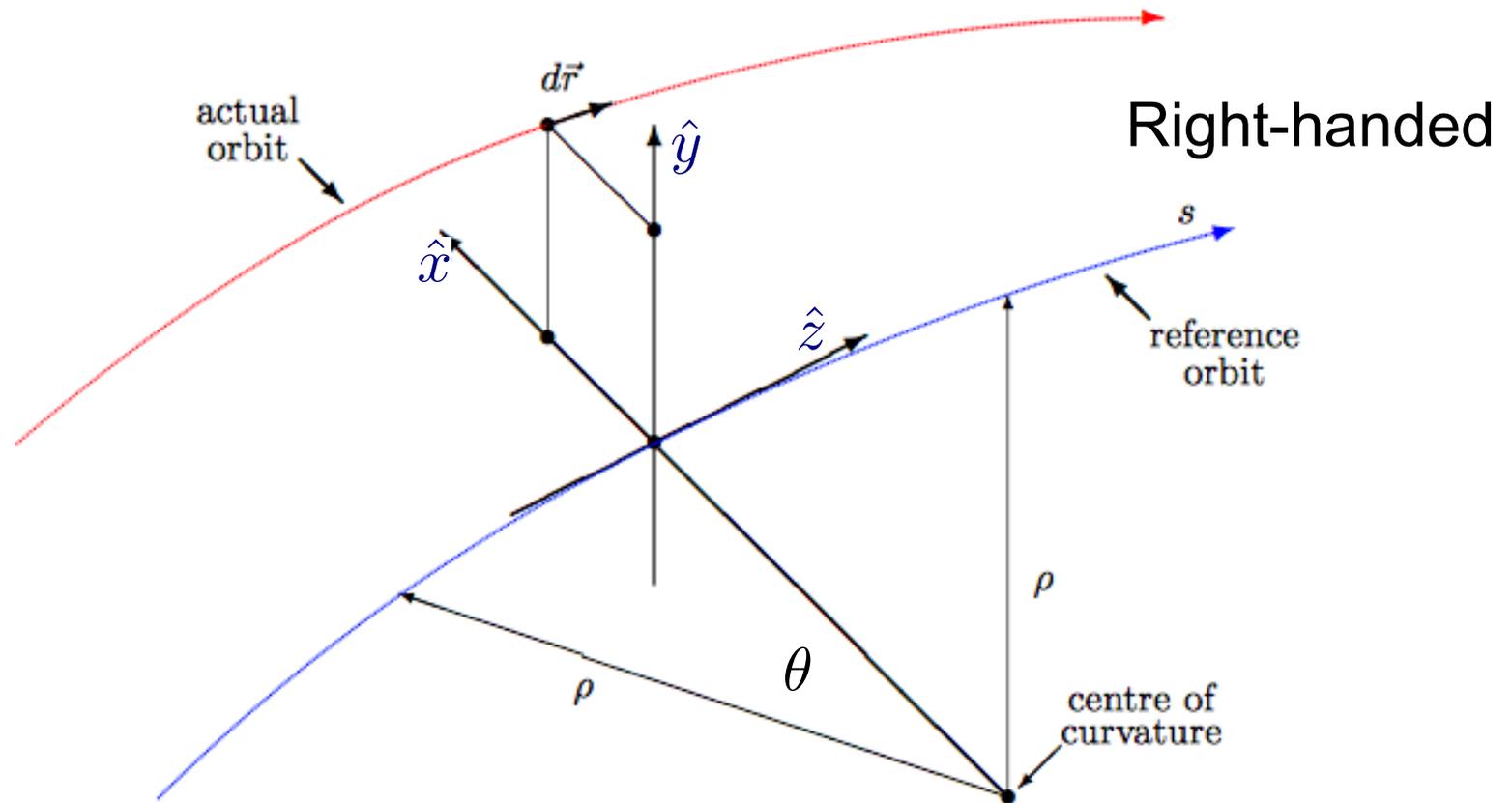
- Also define local trajectory angle

$$x' \equiv \frac{dx}{ds} = \frac{1}{R} \frac{dx}{d\theta} \approx \frac{p_x}{p_0}$$



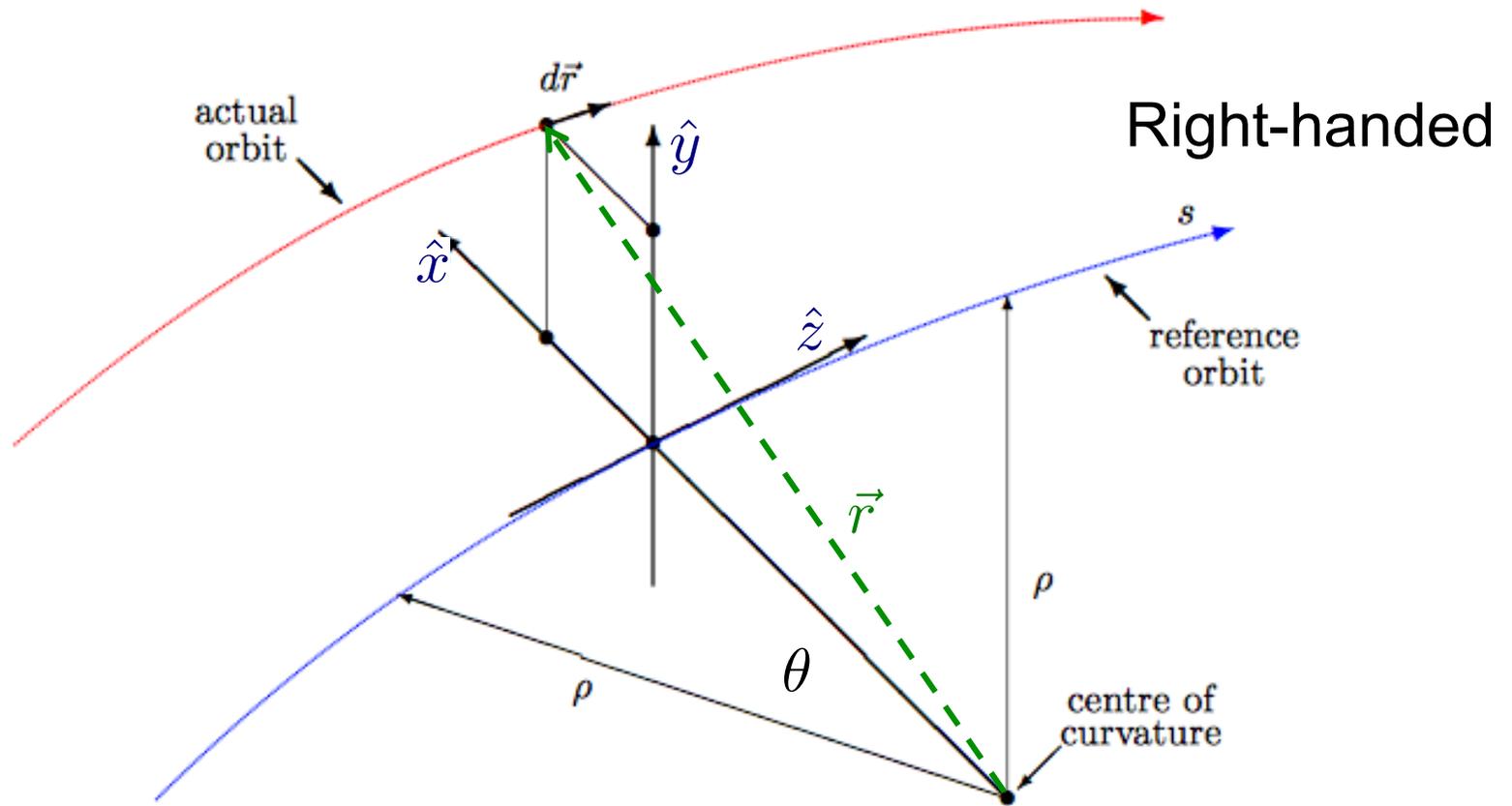
Example: MAD/madx Coordinate System

<http://madx.web.cern.ch/madx/madX/doc/latexuguide/madxuguide.pdf> p.10



Example: MAD/madx Coordinate System

<http://madx.web.cern.ch/madx/madX/doc/latexuguide/madxuguide.pdf> p.10



$$\vec{r} = (\rho + x)\hat{x} + y\hat{y} + z\hat{z}$$

$$R = \rho + x \quad \frac{R}{\rho} = \left(1 + \frac{x}{\rho}\right)$$

2.2: Parameterizing Particle Motion: Approximations

- We will make a few reasonable approximations:

(A0) 0) No local currents (beam travels in a near-vacuum)

(A1) 1) Paraxial approximation: $x', y' \ll 1$ or $p_x, p_y \ll p_0$

(A2) 2) Perturbative coordinates: $x, y \ll \rho$

(A3) 3) *Transverse uncoupled linear magnetic field:*

$$\vec{B} = B_0 \hat{y} + (x \hat{y} + y \hat{x}) \left(\frac{\partial B_y}{\partial x} \right)$$

(A0) Note this obeys Maxwell's equations in free space

(A4) 4) Negligible E field: $\gamma \approx \text{constant}$

- Equivalent to assuming adiabatically changing B fields relative to $dx/dt, dy/dt$

Parameterizing Particle Motion: Acceleration

- Lorentz force equation of motion is

$$q\vec{v} \times \vec{B} = \frac{d(\gamma m \vec{v})}{dt} = \gamma m \dot{\vec{v}} \quad (\text{A4})$$

- Calculate velocity and acceleration in our coordinate system

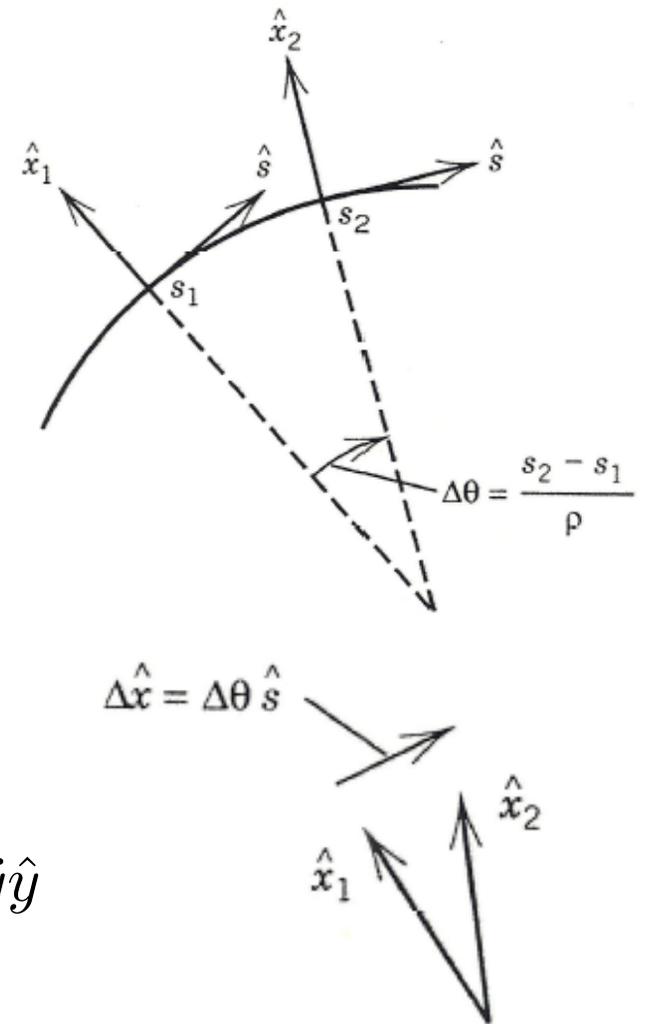
$$\vec{v} = \dot{R}\hat{x} + R\dot{\hat{x}} + \dot{y}\hat{y} = \dot{R}\hat{x} + R\dot{\theta}\hat{s} + \dot{y}\hat{y}$$

$$\dot{\vec{v}} = \ddot{R}\hat{x} + (2\dot{R}\dot{\theta} + R\ddot{\theta})\hat{s} + R\dot{\theta}\dot{\hat{s}} + \ddot{y}\hat{y}$$

$$\dot{\hat{s}} = -\dot{\theta}\hat{x} = -\frac{v}{R}\hat{x}$$

so
$$\dot{\vec{v}} = (\ddot{R} - R\dot{\theta}^2)\hat{x} + (2\dot{R}\dot{\theta} + R\ddot{\theta})\hat{s} + \ddot{y}\hat{y}$$

$$\dot{\vec{v}} = \left(\ddot{x} - \frac{v^2}{R} \right) \hat{x} + \frac{2\dot{x}v}{R} \hat{s} + \ddot{y}\hat{y}$$



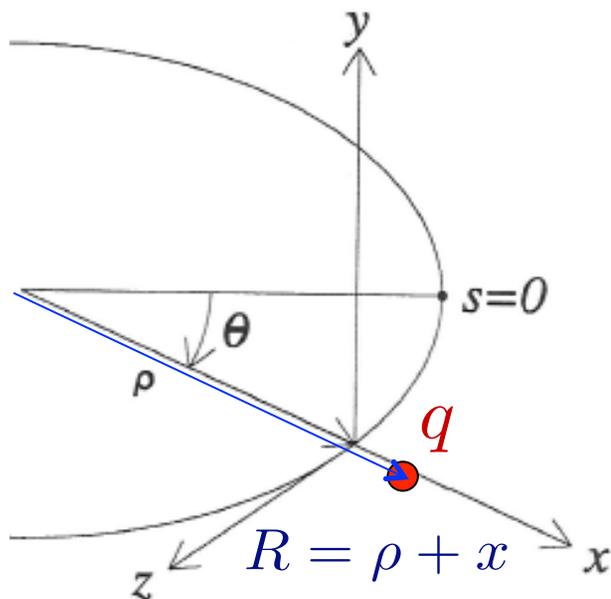
Parameterizing Particle Motion: Eqn of Motion

- Component equations of motion

Vertical: $F_y = q\beta c B_x = \gamma m \ddot{y}$ $\ddot{y} - \frac{q\beta c B_x}{\gamma m} = 0$

$t = \frac{R}{\beta c} \theta \Rightarrow \frac{d}{dt} = \frac{\beta c}{R} \frac{d}{d\theta}$ $\frac{d^2 y}{d\theta^2} - \frac{q B_x}{\beta c \gamma m} R^2 = 0$

$$\frac{d^2 y}{d\theta^2} - \frac{q B_x}{p} R^2 = 0$$



Horizontal: $F_x = -q\beta c B_y = \gamma m \left(\ddot{x} - \frac{v^2}{R} \right)$

$$\frac{d^2 x}{d\theta^2} = -\frac{q B_y R}{p} + R$$

$$\frac{d^2 x}{d\theta^2} + \left(\frac{q B_y}{p} R - 1 \right) R = 0$$

Equations of Motion

- Apply our paraxial and linearization approximations

$$p = qB_0\rho \quad R = \rho \left(1 + \frac{x}{\rho}\right) \quad B_y = B_0 + \left(\frac{\partial B_y}{\partial x}\right)x \quad B_x = \left(\frac{\partial B_y}{\partial x}\right)y$$

Horizontal: $\frac{d^2x}{d\theta^2} + \left(\frac{qB_y}{p}R - 1\right)R = 0$

$$\frac{d^2x}{d\theta^2} + \left[\left(1 + \frac{1}{B_0}\frac{\partial B_y}{\partial x}x\right)\left(1 + \frac{x}{\rho}\right) - 1\right]\rho\left(1 + \frac{x}{\rho}\right) = 0$$

$$\Rightarrow \frac{d^2x}{d\theta^2} + (1 - n)x = 0 \quad \text{where} \quad n \equiv -\frac{\rho}{B_0}\left(\frac{\partial B_y}{\partial x}\right)$$

Vertical: $\frac{d^2y}{d\theta^2} - \frac{qB_x}{p}R^2 = 0 \quad \Rightarrow \frac{d^2y}{d\theta^2} + ny = 0$

Things to try sometime

- Expand the horizontal equation of motion to second order in x
 - Does it reduce to the stated equation at first order?
 - Use expansions for R , B that are still first order!
- Expand the horizontal and vertical equations of motion to second order in x , y , δ (p. 25-6 of these slides)
 - Use expansions for R , B that are still first order!

Simple Equations of Motion!

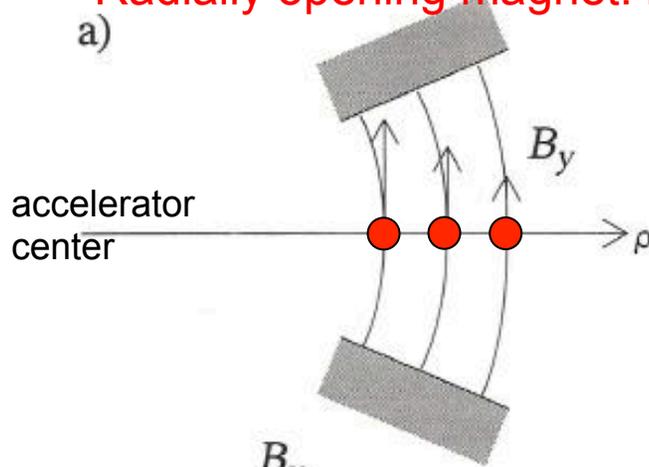
$$\frac{d^2x}{d\theta^2} + (1 - n)x = 0$$

$$\frac{d^2y}{d\theta^2} + ny = 0$$

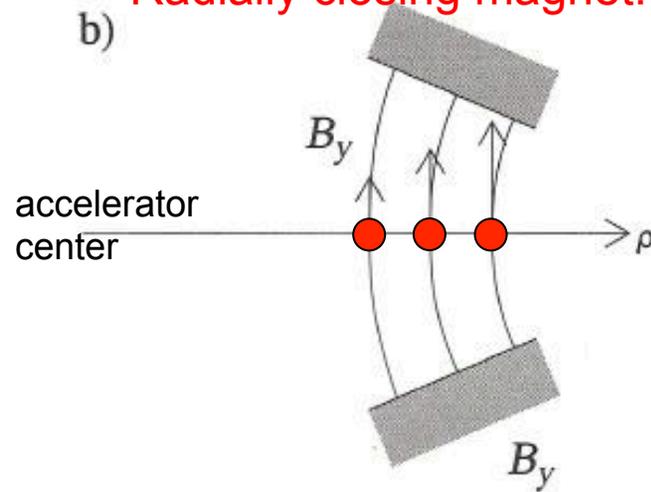
- These are simple harmonic oscillator equations
(Not surprising since we linearized 2nd order differential equations)
- These are known as the **weak focusing** equations
If n does not depend on θ , stability is only possible in both planes if **$0 < n < 1$**
This is known as the **weak focusing criterion**
There is less than one oscillation per 2π in θ

Visualization: Weak Focusing Forces

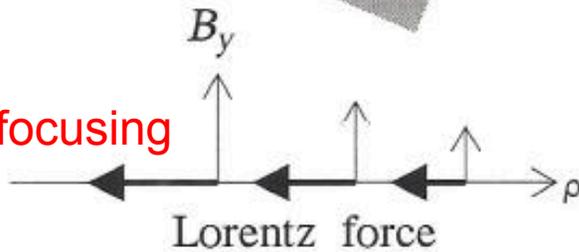
a) Radially opening magnet: $n > 0$



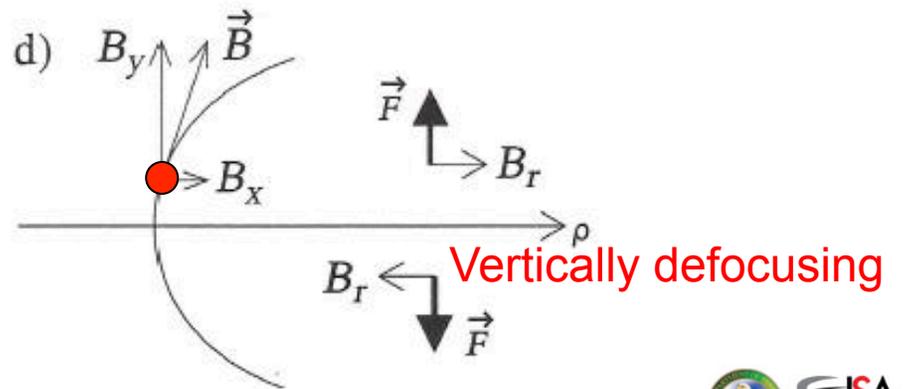
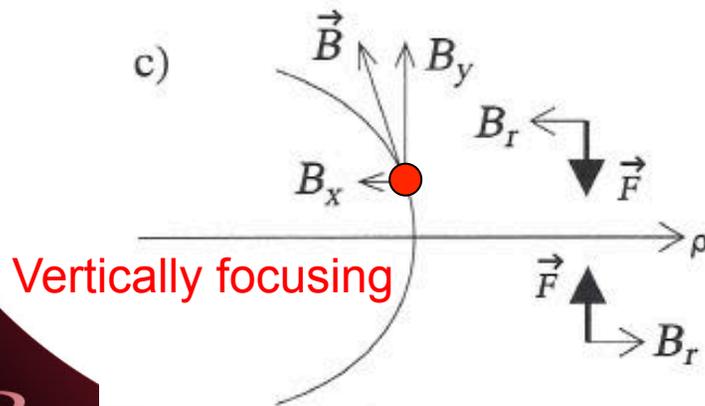
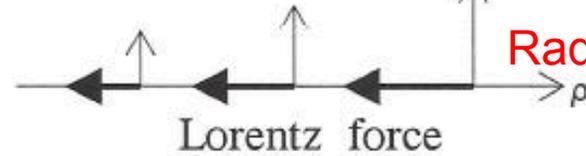
b) Radially closing magnet: $n < 0$



Radially defocusing



Radially focusing



But Wasn't $0 < n < 1$ Stable?

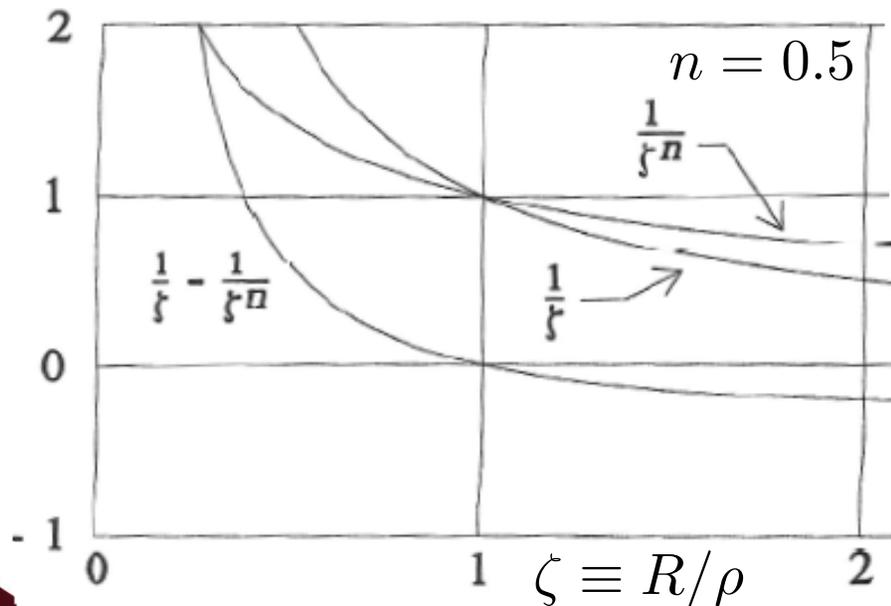
- This seems to indicate $n > 0$ is horizontally unstable!
- Horizontal motion is a combination of two forces

“Centrifugal” mv^2/R and centripetal Lorentz qvB_y

Both forces cancel **by definition** for the design trajectory

$$F_{tot} = \frac{mv^2}{R} - qvB_y \approx \frac{mv^2}{\rho} \left(\frac{\rho}{R}\right) - qvB_0 \left(\frac{\rho}{R}\right)^n = qvB_0 \left(\frac{1}{\zeta} - \frac{1}{\zeta^n}\right)$$

where $\zeta \equiv \frac{R}{\rho}$

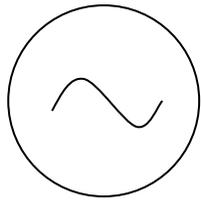


$$F_{tot} > 0 \text{ for } \zeta < 1$$

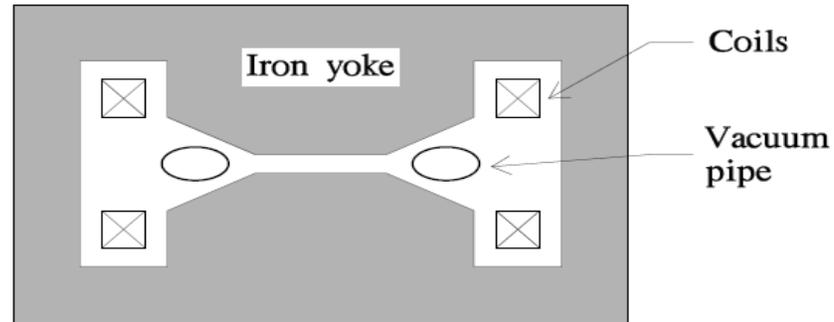
$$F_{tot} < 0 \text{ for } \zeta > 1$$

Nonlinear too! But we linearize near $\zeta=1$

Interlude: The Betatron Again



$$I(t) = I_0 \cos(2\pi\omega_1 t)$$

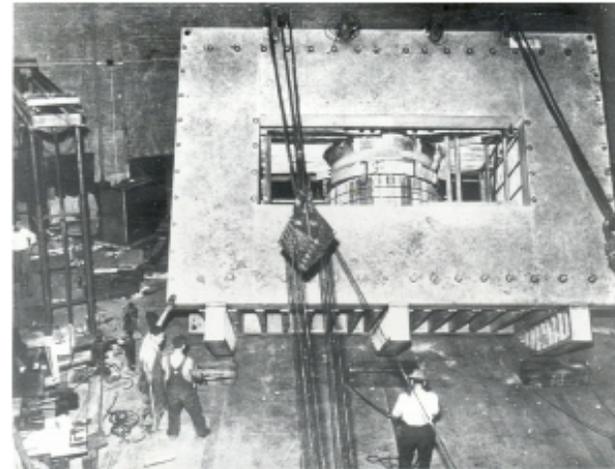


- Weak focusing formalism was originally developed for the Betatron
- Apply Faraday's law with time-varying current in coils
- Beam sees time-varying accelerating electric field too!
- Early proofs of stability: focusing and “betatron” motion

Donald Kerst
UIUC 2.5 MeV
Betatron, 1940



Don't try this at home!!



UIUC 312 MeV
betatron, 1949

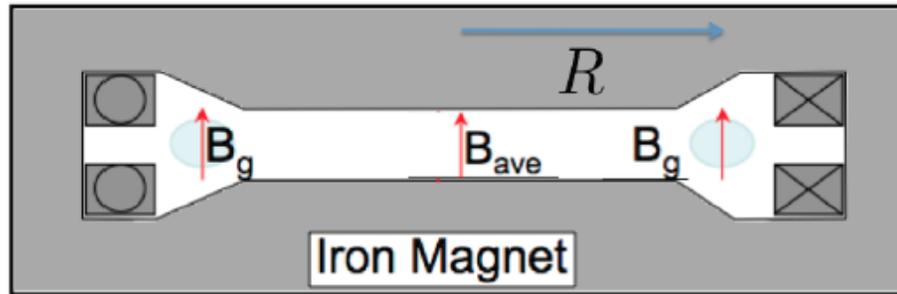
Really don't try this at home!!

Example: The Betatron

apply sinusoidally varying current to toroidal conductors

$$I = I_0 \sin(\omega t)$$

$$B_{\text{ave}} = B_0 \sin(\omega t)$$



cylindrically symmetric about center vertical axis

Magnetic flux $\phi \approx \pi R^2 B_{\text{ave}} = \pi R^2 B_0 \sin(\omega t)$

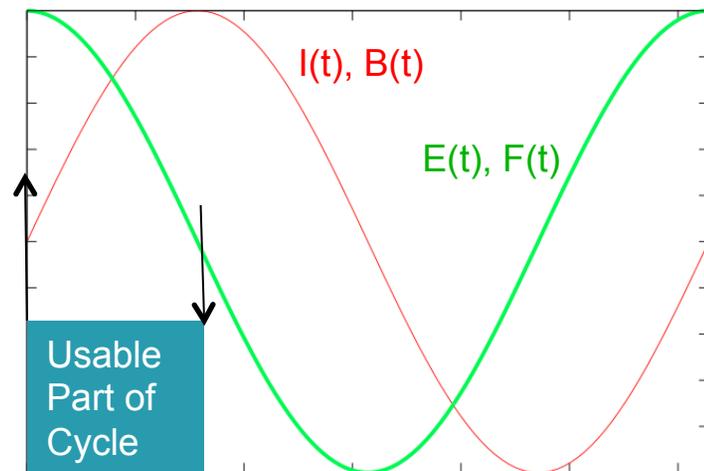
Faraday's law $\mathcal{E} = -\frac{d\phi}{dt} \quad \oint \vec{E} \cdot d\vec{r} = 2\pi R E = -\frac{d\phi}{dt} = -\pi R^2 B_0 \omega \cos(\omega t)$

Force on electron $F = qE = -\frac{qR}{2} \frac{dB_{\text{ave}}}{dt} = \frac{eRB_0\omega}{2} \cos(\omega t)$

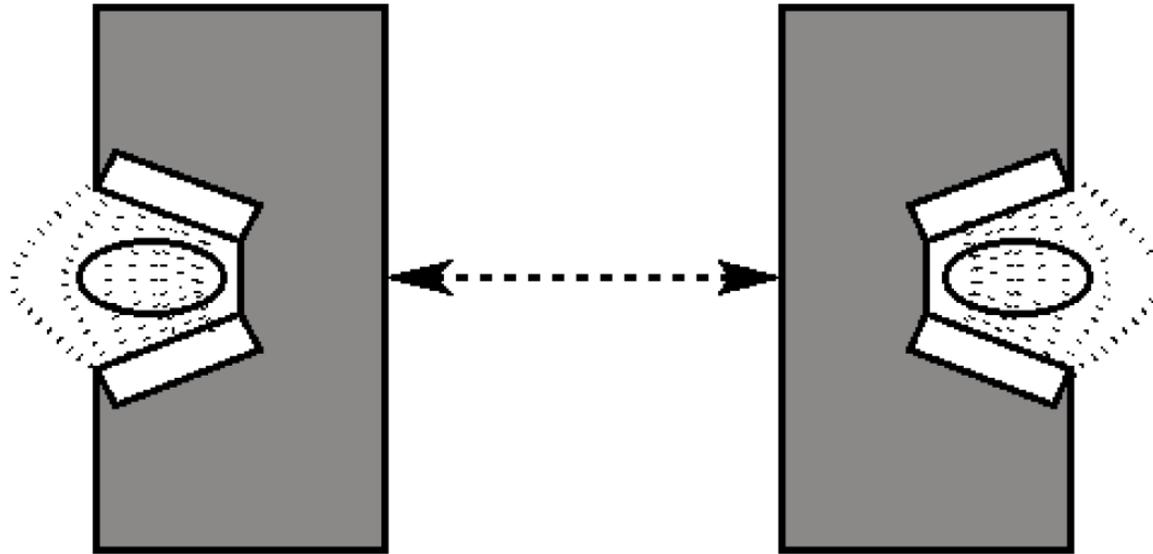
Circular motion

$$p/q = B_g R \Rightarrow F = \frac{dp}{dt} = eR \frac{dB_g}{dt}$$

Betatron Field Condition $B_g = \frac{B_0}{2}$



Example: Synchrotron Weak Focusing



- Separate RF cavities can eliminate the need for central iron (and corresponding huge inductance)
 - Accelerator can be (much) larger (higher energies for same B_0 !)
 - But stability equation scaling with ρ is still not good:

$$0 < -\frac{\rho}{B_0} \left(\frac{\partial B_y}{\partial x} \right)_{x=0} < 1$$

2.3: Back to Solutions of Equations of Motion

$$\frac{d^2x}{d\theta^2} + (1 - n)x = 0 \qquad \frac{d^2y}{d\theta^2} + ny = 0$$

- Assume azimuthal symmetry (n does not depend on θ)
- Solutions are simple harmonic oscillator solutions

$$x(\theta) = A \cos(\theta\sqrt{1-n}) + B \sin(\theta\sqrt{1-n})$$

$$\frac{dx}{d\theta} = \sqrt{1-n}[-A \sin(\theta\sqrt{1-n}) + B \cos(\theta\sqrt{1-n})]$$

- Constants A, B are related to initial conditions (x_0, x'_0)

$$x_0 = x(\theta = 0) = A \qquad x'_0 = \frac{1}{\rho} \left(\frac{dx}{d\theta} \right) (\theta = 0) = \frac{\sqrt{1-n}}{\rho} B$$

$$A = x_0 \qquad B = \frac{\rho}{\sqrt{1-n}} x'_0$$

Solutions of Equations of Motion

- Write down solutions in terms of initial conditions

$$x(\theta) = \cos(\theta\sqrt{1-n}) x_0 + \frac{\rho}{\sqrt{1-n}} \sin(\theta\sqrt{1-n}) x'_0$$

$$x'(\theta) = \frac{1}{\rho} \frac{dx}{d\theta} = -\frac{\sqrt{1-n}}{\rho} \sin(\theta\sqrt{1-n}) x_0 + \cos(\theta\sqrt{1-n}) x'_0$$

- This can be (very) conveniently written as matrices (including both horizontal and vertical)

$$\begin{pmatrix} x(\theta) \\ x'(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{1-n}) & \frac{\rho}{\sqrt{1-n}} \sin(\theta\sqrt{1-n}) \\ -\frac{\sqrt{1-n}}{\rho} \sin(\theta\sqrt{1-n}) & \cos(\theta\sqrt{1-n}) \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$$
$$\begin{pmatrix} y(\theta) \\ y'(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{n}) & \frac{\rho}{\sqrt{n}} \sin(\theta\sqrt{n}) \\ -\frac{\sqrt{n}}{\rho} \sin(\theta\sqrt{n}) & \cos(\theta\sqrt{n}) \end{pmatrix} \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix}$$

Transport Matrices

$$\begin{pmatrix} y(\theta) \\ y'(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{n}) & \frac{\rho}{\sqrt{n}} \sin(\theta\sqrt{n}) \\ -\frac{\sqrt{n}}{\rho} \sin(\theta\sqrt{n}) & \cos(\theta\sqrt{n}) \end{pmatrix} \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix} = M_V(\theta) \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix}$$

- M_V here is an example of a **transport matrix**

- **Linear**: derived from linear equations

- Can be concatenated to make further transformations

$$M_V(\theta_1 + \theta_2) = M_V(\theta_2)M_V(\theta_1)$$

Note order

- Depends only on “length” θ , radius ρ , and “field” n

- Acts to transform or transport coordinates to a new state
- Our accelerator “lattices” will be built out of these matrices

- **Unimodular**: $\det(M_V)=1$

- More strongly, it's symplectic: $S = M_V^T S M_V$ where $S = \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix}$
- Hamiltonian dynamics, phase space conservation (Liouville)
- These matrices here are scaled rotations!

Sinusoidal Solutions, Betatron Phases

$$\begin{pmatrix} x(\theta) \\ x'(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{1-n}) & \frac{\rho}{\sqrt{1-n}} \sin(\theta\sqrt{1-n}) \\ -\frac{\sqrt{1-n}}{\rho} \sin(\theta\sqrt{1-n}) & \cos(\theta\sqrt{1-n}) \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$$

$$\begin{pmatrix} y(\theta) \\ y'(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{n}) & \frac{\rho}{\sqrt{n}} \sin(\theta\sqrt{n}) \\ -\frac{\sqrt{n}}{\rho} \sin(\theta\sqrt{n}) & \cos(\theta\sqrt{n}) \end{pmatrix} \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix}$$

- Sinusoidal simple harmonic oscillators solutions
 - Particles move in transverse **betatron oscillations** around the **design trajectory** $(x, x') = (y, y') = 0$
- We define **betatron phases**

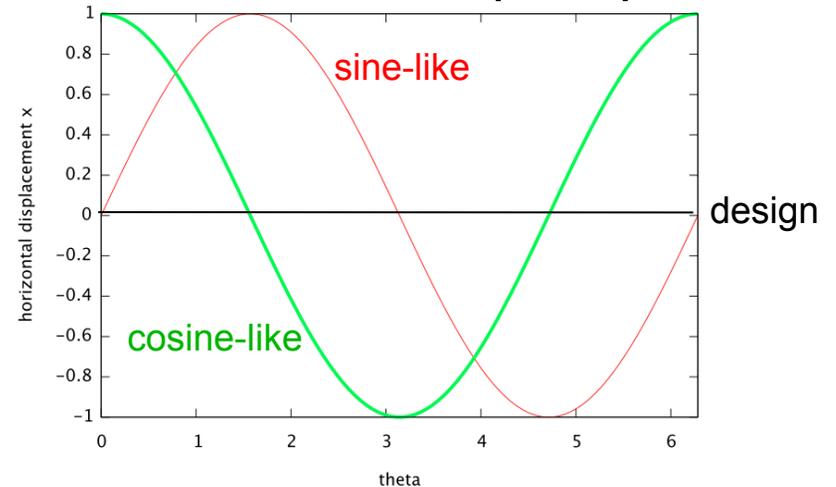
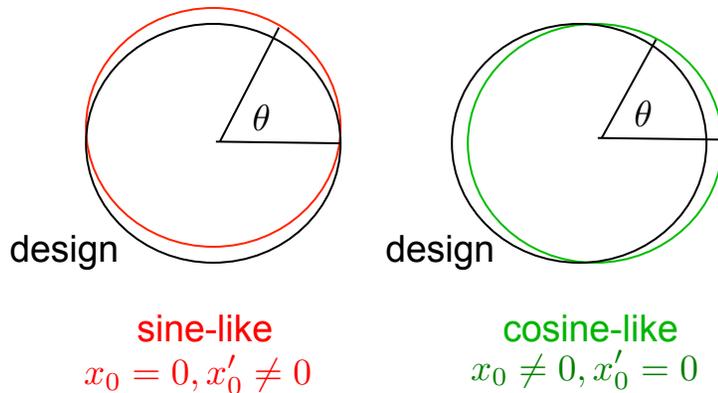
$$\phi_x(s) \equiv \theta\sqrt{1-n} = \frac{s}{\rho}\sqrt{1-n} \quad \phi_y(s) \equiv \theta\sqrt{n} = \frac{s}{\rho}\sqrt{n}$$

Write matrix equation in terms of s rather than θ

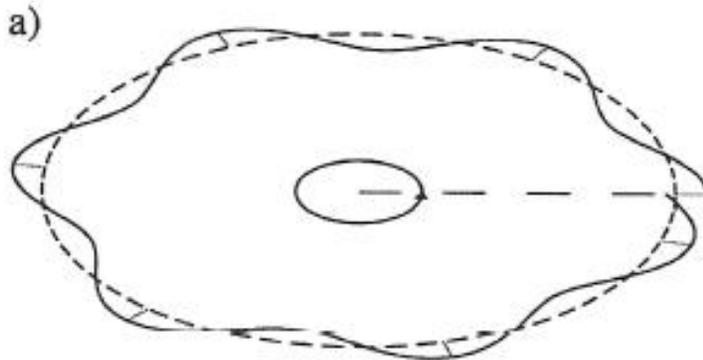
$$\begin{pmatrix} x(s) \\ x'(s) \end{pmatrix} = \begin{pmatrix} \cos \phi_x(s) & \frac{\rho}{\sqrt{1-n}} \sin \phi_x(s) \\ -\frac{\sqrt{1-n}}{\rho} \sin \phi_x(s) & \cos \phi_x(s) \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$$

Visualization of Betatron Oscillations

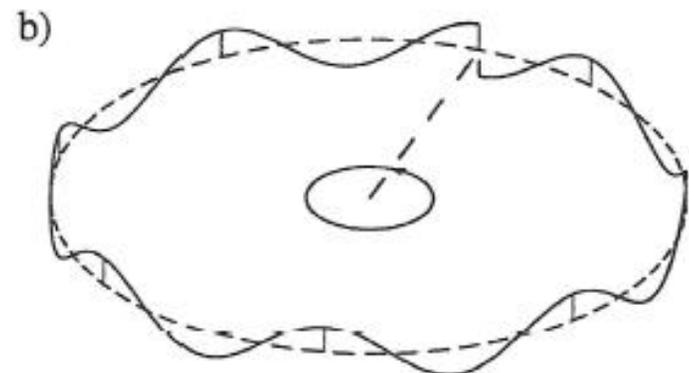
- Simplest case: constant uniform vertical field ($n=0$)



- More complicated **strong focusing**



Horizontal Betatron Oscillation
with tune: $Q_h = 6.3$,
i.e., 6.3 oscillations per turn.



Vertical Betatron Oscillation
with tune: $Q_v = 7.5$,
i.e., 7.5 oscillations per turn.

Visualization of Betatron Oscillations, Tunes

- What happens for $0 < n < 1$?
 - Example picture below has 5 “turns” with $\sin(0.89 \theta)$
 - The betatron oscillation precesses, not strictly periodic
 - Betatron tune $Q_{x,y}$** : number of cycles made for every revolution or turn around accelerator

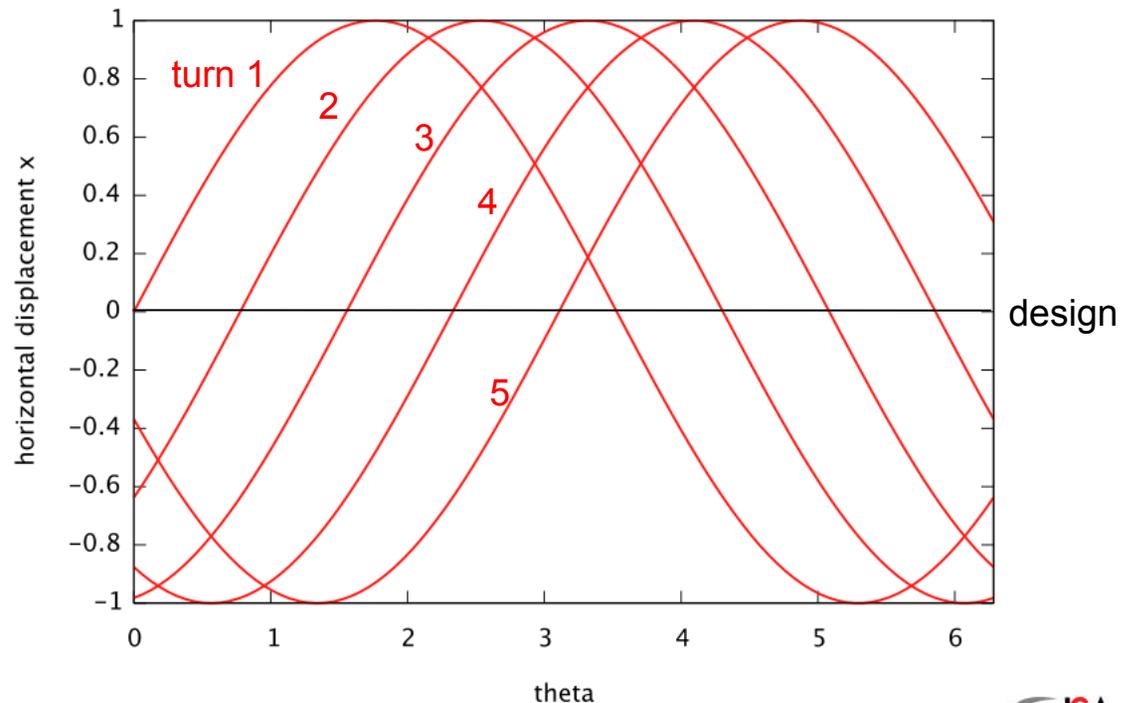
$$Q_x = \frac{1}{2\pi} \sqrt{1-n} (2\pi) = \sqrt{1-n}$$

$$Q_y = \frac{1}{2\pi} \sqrt{n} (2\pi) = \sqrt{n}$$

Frequency of betatron oscillations relative to turns around accelerator

For weak focusing:

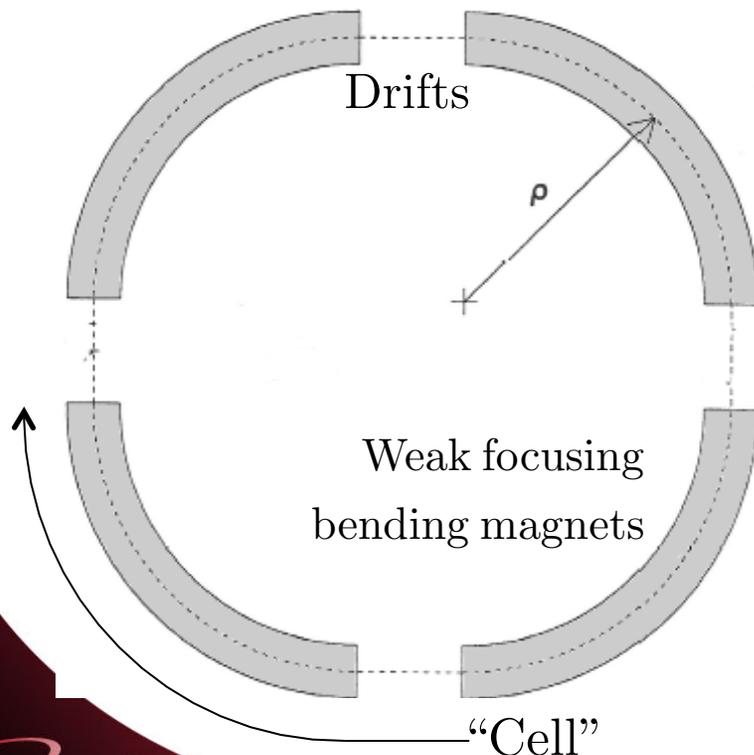
$$Q_x^2 + Q_y^2 = 1$$



Transport Matrices: Piecewise Solutions

$$\begin{pmatrix} y(\theta) \\ y'(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{n}) & \frac{\rho}{\sqrt{n}} \sin(\theta\sqrt{n}) \\ -\frac{\sqrt{n}}{\rho} \sin(\theta\sqrt{n}) & \cos(\theta\sqrt{n}) \end{pmatrix} \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix} = M_V(\theta) \begin{pmatrix} y_0 \\ y'_0 \end{pmatrix}$$

- Linear transport matrices make piecewise solutions of equations of motion accessible



“Cell” transport matrix:

$$M_{\text{cell}} = M(\theta) M_{\text{drift}}$$

“One turn” transport matrix:

$$M_{\text{one turn}} = (M(\theta) M_{\text{drift}})^4$$

Build accelerator optics out of
“Lego” transport matrices
(everything is awesome!)



Transport Matrices: Accelerator Legos

(A3)

- With linear fields, there are two basic types of Legos

- Dipoles**

$$\vec{B} = B_0 \hat{y} + (x \hat{y} + y \hat{x}) \left(\frac{\partial B_y}{\partial x} \right) \quad B_0 \neq 0$$

- Often long magnets to bend design trajectory
- Entrance/exit locations can become important
- May or may not include focusing (“combined function”)
- Special case: drift when all B components are zero

- Quadrupoles**

$$\vec{B} = (x \hat{y} + y \hat{x}) \left(\frac{\partial B_y}{\partial x} \right) \quad B_0 = 0$$

- Design trajectory is straight! (no fields at x=y=0)
- Act to focus particles moving off of design trajectory
- Special case: “thin lens” approximation
- We’ ll talk about quadrupoles tomorrow

Transport Matrices: Dipole

- We have already derived a very general **transport matrix for a dipole magnet with focusing**

$$\begin{pmatrix} x(s) \\ x'(s) \\ y(s) \\ y'(s) \end{pmatrix} = \begin{pmatrix} \cos \phi_x(s) & \frac{\rho}{\sqrt{1-n}} \sin \phi_x(s) & 0 & 0 \\ -\frac{\sqrt{1-n}}{\rho} \sin \phi_x(s) & \cos \phi_x(s) & 0 & 0 \\ 0 & 0 & \cos \phi_y(s) & \frac{\rho}{\sqrt{n}} \sin \phi_y(s) \\ 0 & 0 & -\frac{\sqrt{n}}{\rho} \sin \phi_y(s) & \cos \phi_y(s) \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \\ y_0 \\ y'_0 \end{pmatrix}$$

$$\phi_x(s) \equiv \theta \sqrt{1-n} = \frac{s}{\rho} \sqrt{1-n} \quad \phi_y(s) \equiv \theta \sqrt{n} = \frac{s}{\rho} \sqrt{n}$$

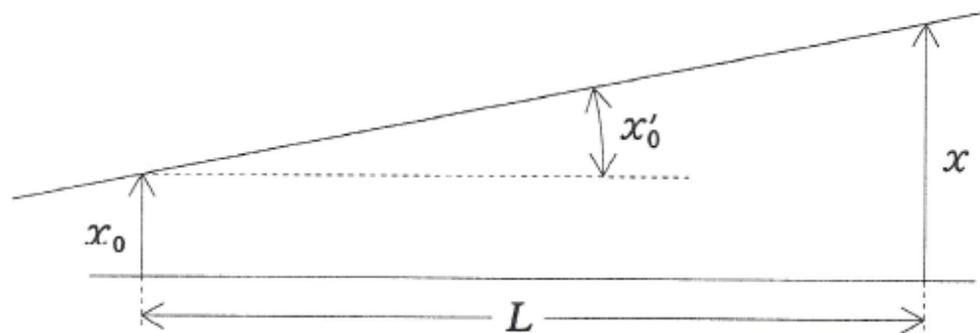
- Taking $n \rightarrow 0$ (and being careful) gives the **transport matrix for a dipole of bend angle θ without focusing**

$$\begin{pmatrix} x(s) \\ x'(s) \\ y(s) \\ y'(s) \end{pmatrix} = \begin{pmatrix} \cos \theta & \rho \sin \theta & 0 & 0 \\ -\frac{1}{\rho} \sin \theta & \cos \theta & 0 & 0 \\ 0 & 0 & 1 & \rho \theta \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \\ y_0 \\ y'_0 \end{pmatrix}$$

Transport Matrices: Drifts

$$\begin{pmatrix} x(s) \\ x'(s) \\ y(s) \\ y'(s) \end{pmatrix} = \begin{pmatrix} \cos \theta & \rho \sin \theta & 0 & 0 \\ -\frac{1}{\rho} \sin \theta & \cos \theta & 0 & 0 \\ 0 & 0 & 1 & \rho\theta \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \\ y_0 \\ y'_0 \end{pmatrix}$$

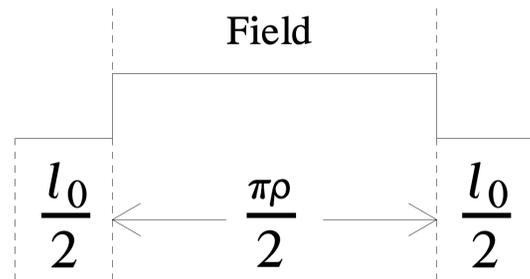
- For $n=0$, there is no horizontal field or vertical force
 - The vertical transport matrix here is for a **field-free drift**
 - This applies in both x,y planes when there is no field



$$\begin{pmatrix} x(s) \\ x'(s) \end{pmatrix} = \begin{pmatrix} 1 & L \\ 0 & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$$

2.5: Weak Focusing Synchrotron

- Back to our Lego machine
- Pick a more symmetric cell



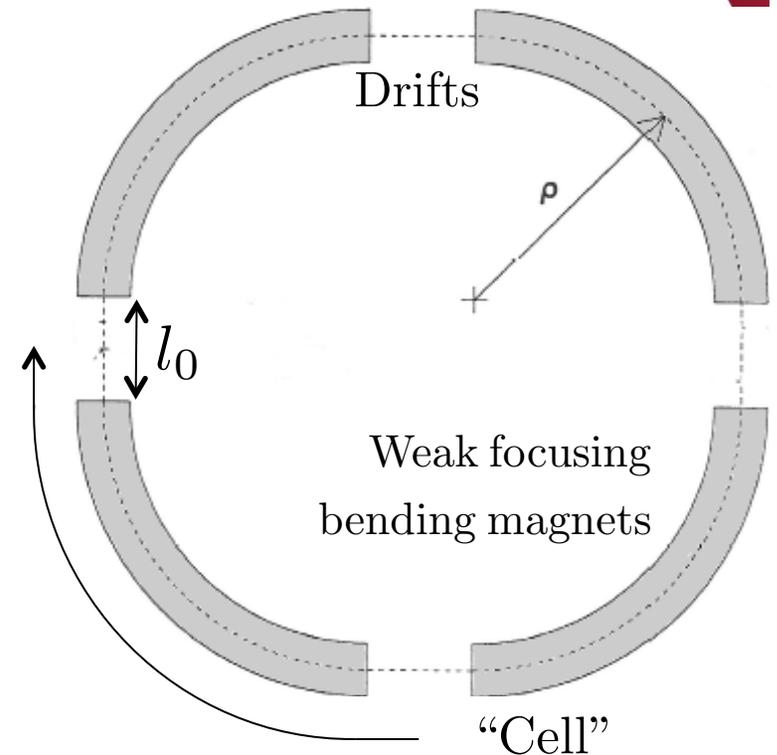
$$M_H = M_{\text{drift}} \left(\frac{l_0}{2} \right) M_{\text{dipole}} \left(\frac{\pi}{2} \right) M_{\text{drift}} \left(\frac{l_0}{2} \right)$$

- For $l_0 \ll \pi\rho$ “one can show”

$$\text{Phase advance per cell : } \mu_H = \left(1 + \frac{l_0}{\pi\rho} \right) \frac{\pi\sqrt{1-n}}{2}$$

$$\text{Horizontal tune : } Q_H = \frac{4\mu_H}{2\pi} = \left(1 + \frac{l_0}{\pi\rho} \right) \sqrt{1-n}$$

$$\text{Vertical tune : } Q_V = \left(1 + \frac{l_0}{\pi\rho} \right) \sqrt{n}$$



$$\text{Circumference } C = 2\pi\rho + 4l_0$$

Weak Focusing Synchrotron Parameterization

- We can write the cell transport matrix M_H in a form that is very similar to a rotation matrix

$$M_H = \begin{pmatrix} \cos \mu_H & \beta_H \sin \mu_H \\ -\frac{1}{\beta_H} \sin \mu_H & \cos \mu_H \end{pmatrix}$$

- We will investigate this parameterization (and its non-periodic lattice extensions) extensively later this week
- β_H is a length scale for the betatron oscillations
- Details in Section 2.5 derive:

$$\beta_H \approx \frac{\rho}{\sqrt{1-n}} \left(1 + \frac{l_0}{\pi\rho} \right) \quad \beta_V \approx \frac{\rho}{\sqrt{n}} \left(1 + \frac{l_0}{\pi\rho} \right)$$

- Note the familiar scaling with the radius of curvature ρ !

2.4: What About Momentum?

- So far we have assumed that the design trajectory particle and our particle have the **same momentum**
- How do equations change if we break this assumption?
 - Expect only horizontal motion changes to first order (A2)

$$p = p_0(1 + \delta) \text{ where } \delta \equiv \frac{\Delta p}{p_0} \ll 1 \quad p_0 = \text{design particle momentum}$$

$$\frac{d^2x}{d\theta^2} + \left(\frac{qB_y}{p} R - 1 \right) R = 0 \quad \Rightarrow \quad \frac{d^2x}{d\theta^2} + \left(\frac{qB_y}{p_0(1 + \delta)} R - 1 \right) R = 0$$

$$\frac{d^2x}{d\theta^2} + \left(\frac{qB_y}{p_0} (1 - \delta) R - 1 \right) R = 0 \quad \text{(A1)}$$

$$\frac{d^2x}{d\theta^2} + \left(\frac{qB_y}{p_0} R - 1 \right) R = \delta \frac{R^2 qB_y}{p_0} = \rho\delta \quad \text{(A2)}$$

$$\frac{d^2x}{d\theta^2} + (1 - n)x = \rho\delta$$

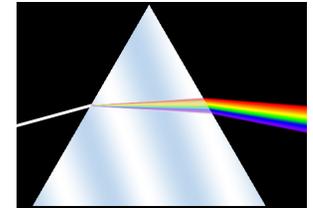
Add inhomogeneous term to original $\delta=0$ equation of motion

Solutions of Dispersive Equations of Motion

$$\frac{d^2x}{d\theta^2} + (1 - n)x = \rho\delta$$

$$\frac{d^2y}{d\theta^2} + ny = 0$$

- This momentum effect is called **dispersion**
 - Similar to prism light dispersion in classical optics
- Solutions are simple harmonic oscillator solutions
 - But now we add a specific inhomogeneous solution



$$x(\theta) = A \cos(\theta\sqrt{1 - n}) + B \sin(\theta\sqrt{1 - n}) + \frac{\rho}{1 - n}\delta \quad \text{inhomogeneous term!}$$

$$\frac{dx}{d\theta} = \sqrt{1 - n}[-A \sin(\theta\sqrt{1 - n}) + B \cos(\theta\sqrt{1 - n})]$$

- Constants A,B again related to initial conditions (x_0, x'_0)

$$A = x_0 - \frac{\rho}{1 - n}\delta \quad B = \frac{\rho}{\sqrt{1 - n}}x'_0$$

δ is constant (A4)

Solutions of Dispersive Equations of Motion

- Write down solutions in terms of initial conditions

$$x'(\theta) = -\frac{\sqrt{1-n}}{\rho} \sin(\theta\sqrt{1-n})x_0 + \cos(\theta\sqrt{1-n})x'_0 + \frac{1}{\sqrt{1-n}} \sin(\theta\sqrt{1-n})\delta_0$$

$$x'(\theta) = \frac{1}{\rho} \frac{dx}{d\theta} = -\frac{\sqrt{1-n}}{\rho} \sin(\theta\sqrt{1-n})x_0 + \cos(\theta\sqrt{1-n})x'_0 + \frac{1}{\sqrt{1-n}} \sin(\theta\sqrt{1-n})\delta_0$$

$$\delta = \delta_0$$

- This can be now be “conveniently” written in terms of a 3x3 matrix:

$$\begin{pmatrix} x(\theta) \\ x'(\theta) \\ \delta(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{1-n}) & \frac{\rho}{\sqrt{1-n}} \sin(\theta\sqrt{1-n}) & \frac{\rho}{1-n} [1 - \cos(\theta\sqrt{1-n})] \\ -\frac{\sqrt{1-n}}{\rho} \sin(\theta\sqrt{1-n}) & \cos(\theta\sqrt{1-n}) & \frac{1}{\sqrt{1-n}} \sin(\theta\sqrt{1-n}) \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \\ \delta_0 \end{pmatrix}$$

As usual, this can be simplified for n=0 (pure dipole)

Note that δ has become a “coordinate”!

Sector Dipole Magnets

- This transport matrix applies for **any** angle θ
- So it is also the transport matrix of any section of constant field, and now includes dispersion.
 - In particular, it is the horizontal transport for a **combined function sector dipole** of length $L = \rho\theta$
 - With $n=0$ this is the horizontal transport for a **sector dipole** of length $L = \rho\theta$, bend angle θ , and radius of curvature ρ

$$\mathbf{M}_{\text{dipole}} = \begin{pmatrix} \cos \theta & \rho \sin \theta & \rho(1 - \cos \theta) \\ -\frac{1}{\rho} \sin \theta & \cos \theta & \sin \theta \\ 0 & 0 & 1 \end{pmatrix}$$

- Sector dipole: design trajectory at entrance and exit of magnet is perpendicular to magnet face

Example: 180 Degree Dipole Magnet

$$\begin{pmatrix} x(\theta) \\ x'(\theta) \\ \delta(\theta) \end{pmatrix} = \begin{pmatrix} \cos(\theta\sqrt{1-n}) & \frac{\rho}{\sqrt{1-n}} \sin(\theta\sqrt{1-n}) & \frac{\rho}{1-n} [1 - \cos(\theta\sqrt{1-n})] \\ -\frac{\sqrt{1-n}}{\rho} \sin(\theta\sqrt{1-n}) & \cos(\theta\sqrt{1-n}) & \frac{1}{\sqrt{1-n}} \sin(\theta\sqrt{1-n}) \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \\ \delta_0 \end{pmatrix}$$

$$n = 0 \Rightarrow M_H(\theta) = \begin{pmatrix} \cos \theta & \rho \sin \theta & \rho(1 - \cos \theta) \\ -\frac{1}{\rho} \sin \theta & \cos \theta & \sin \theta \\ 0 & 0 & 1 \end{pmatrix}$$

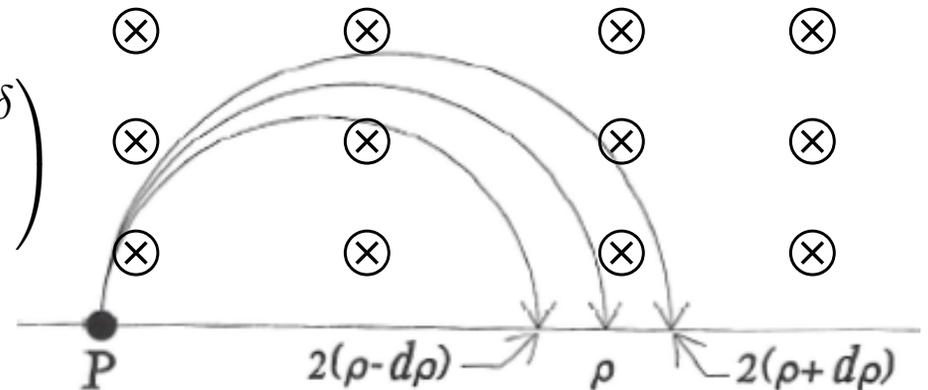
$$n = 0, \theta = \pi \Rightarrow M_H(\theta) = \begin{pmatrix} -1 & 0 & 2\rho \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

For initial coordinates $\begin{pmatrix} 0 \\ 0 \\ \pm\delta \end{pmatrix}$

$$\begin{pmatrix} x \\ x' \\ \delta \end{pmatrix} = \begin{pmatrix} -1 & 0 & 2\rho \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 0 \\ 0 \\ \pm\delta \end{pmatrix} = \begin{pmatrix} \pm 2\rho\delta \\ 0 \\ \pm\delta \end{pmatrix}$$

This makes sense from $p/q = B\rho$!

electrons moving through uniform vertical B field



2.6: Momentum Compaction

- Different momenta particles will have different path lengths $L \equiv \oint ds$ around the accelerator
 - Naively larger $p \rightarrow$ larger $\rho \rightarrow$ larger L
 - This is not necessarily true (as we'll see!)
- This is quantified by a quantity called **momentum compaction**
 - Ratio of fractional change in pathlength to fractional change in momentum

$$\alpha_p \equiv \frac{(dL/L)}{(dp/p)} = \frac{p}{L} \frac{dL}{dp}$$

$$\text{recall } \delta \equiv \frac{dp}{p}$$

Transition Energy

- Relativistic particle motion in a periodic accelerator (like a synchrotron) creates some weird effects
 - For particles moving around with frequency ω in circumference C

$$\omega = \frac{2\pi\beta c}{C} \Rightarrow \frac{d\omega}{\omega} = \frac{d\beta}{\beta} - \frac{dC}{C} = \left(\frac{1}{\gamma^2} - \frac{1}{\gamma_{tr}^2} \right) \delta$$

momentum compaction $\alpha_p \equiv \frac{dC}{C} / \delta = \frac{p}{C} \frac{dC}{dp}$ transition gamma $\gamma_{tr} \equiv \frac{1}{\sqrt{\alpha_p}}$

- At “transition”, $\gamma = \gamma_{tr}$ and **particle revolution frequency does not depend on its momentum**

Reminiscent of a cyclotron but now we're strong focusing and at constant radius!

electron ring

At $\gamma_r > \gamma_{tr}$ higher momentum gives **lower** revolution frequency

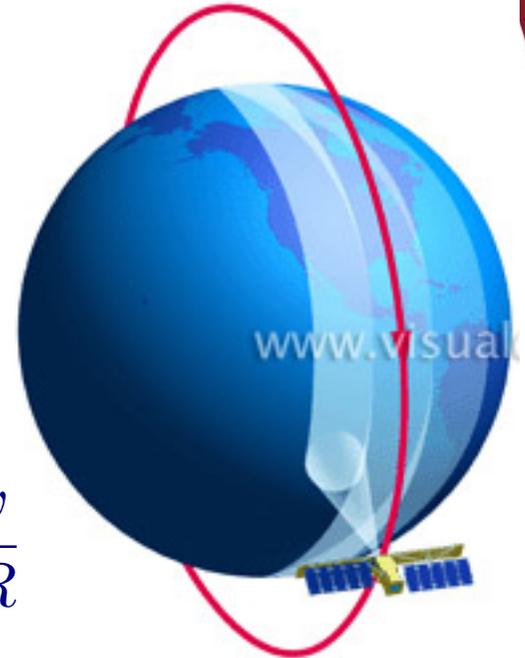
electron linac

At $\gamma_r < \gamma_{tr}$ higher momentum gives **higher** revolution frequency

Hadron synchrotrons can accelerate through transition!

Momentum Compaction: A Classic Example

- Consider a satellite in circular orbit
- A classical gravity/centripetal force problem



$$F = \frac{GMm}{R^2} = \frac{mv^2}{R}$$

$$\frac{GM}{R} = v^2 \quad \omega = 2\pi f = 2\pi \left(\frac{v}{2\pi R} \right) = \frac{v}{R}$$

$$\text{momentum compaction} \quad \alpha_p \equiv \frac{dC}{C} \bigg/ \frac{dp}{p} = \frac{dR}{R} \bigg/ \frac{dv}{v} = \frac{v}{R} \bigg/ \frac{dv}{dR}$$

$$2v \, dv = -\frac{GM}{R^2} dR \quad \Rightarrow \quad \frac{dv}{dR} = -\frac{v}{2R}$$

$$\text{momentum compaction } \alpha_p = -2$$

Raising momentum p **lowers** orbit radius, raises angular frequency ω

Momentum Compaction: Weak Focusing Synchrotron

- Recall $\frac{p}{q} = B\rho$

$$\frac{dp}{p} = \delta = \frac{d\rho}{\rho} + \frac{dB}{B} = \left(1 + \frac{\rho}{B} \frac{\partial B}{\partial \rho}\right) \frac{d\rho}{\rho}$$

$$\delta = (1 - n) \frac{d\rho}{\rho}$$

$$n \equiv -\frac{\rho}{B_0} \left(\frac{\partial B_y}{\partial x}\right)$$

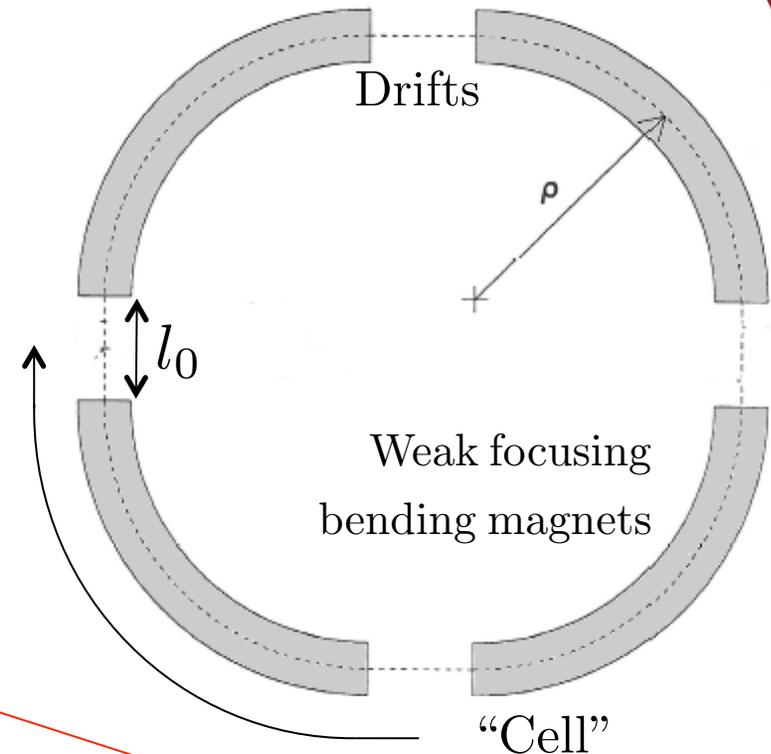
- Now

$$\alpha_p \equiv \frac{dC/C}{dp/p} = \frac{(dC/d\rho)(d\rho/C)}{\delta}$$

$$= \frac{2\pi\rho}{C(1-n)} = \left(1 + \frac{2l_0}{\pi\rho}\right)^{-1} (1-n)^{-1}$$

$$\text{Horizontal tune : } Q_H = \frac{4\mu_H}{2\pi} = \left(1 + \frac{l_0}{\pi\rho}\right) \sqrt{1-n}$$

$$\alpha_p \approx Q_H^{-2}$$



Circumference
 $C = 2\pi\rho + 4l_0$