## USPAS Accelerator Physics 2017 University of California, Davis

# **Chapter 5: Strong Focusing**

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Happy Birthday to Yoichiro Nambu, Paul Ehrenfest, AA Milne, and Cary Grant! Happy National Peking Duck Day, Thesaurus Day, and Winnie the Pooh Day!



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# **Overview**

- Doublets and simple focusing
- 5.1: Transfer matrix approach and linear stability
- 5.2: Analytical approach
- 5.3: Emittances (revisit Friday PM)
- 5.4: Adiabatic Invariants
- 5.5: Dispersion

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- 5.6: Momentum compaction
- Solutions to some problems

# **Strong Focusing**

- String magnets together and look at optical systems
- Real transport systems are generally made of long repeated periods of magnet groups
  - Keep beam together while getting from here to there
- Fundamental problems

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- Quadrupoles (linear focusing) defocus in opposite plane
- Focusing in both planes with weak focusing is too weak
- How do we build a focusing system out of magnets and drifts that we know about?
  - Easiest analysis: string together transport matrices



#### **Magnet Transport Matrix Review**

Drift 
$$\begin{pmatrix} x \\ x' \end{pmatrix}_2 = \begin{pmatrix} 1 & L \\ 0 & 1 \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}_1$$

Thick quadrupole

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{2} = \begin{pmatrix} \cos\sqrt{kl} & \frac{1}{\sqrt{k}}\sin\sqrt{kl} \\ -\sqrt{k}\sin\sqrt{kl} & \cos\sqrt{kl} \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}_{1} & \begin{pmatrix} y \\ y' \end{pmatrix}_{2} = \begin{pmatrix} \cosh\sqrt{kl} & \frac{1}{\sqrt{k}}\sinh\sqrt{kl} \\ \sqrt{k}\sinh\sqrt{kl} & \cosh\sqrt{kl} \end{pmatrix} \begin{pmatrix} y \\ y' \end{pmatrix}_{1}$$

$$\begin{array}{c} \text{Thin quadrupole} \\ \mathbf{f}=(\mathsf{kl})^{-1} > \mathsf{length} \mathsf{I} & \begin{pmatrix} x \\ x' \end{pmatrix}_{2} = \begin{pmatrix} 1 & 0 \\ \mp kl & 1 \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}_{1} = \begin{pmatrix} 1 & 0 \\ \mp \frac{1}{f} & 1 \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}_{1}$$

Sector dipole of bend angle  $\theta$  and radius  $\rho$ 

$$\begin{pmatrix} x \\ x' \\ y \\ y' \\ z \\ \delta \end{pmatrix}_{2} = \begin{pmatrix} \cos\theta & \rho\sin\theta & 0 & 0 & 0 & \rho(1-\cos\theta) \\ -\frac{1}{\rho}\sin\theta & \cos\theta & 0 & 0 & 0 & \sin\theta \\ 0 & 0 & 1 & \rho\theta & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ -\sin\theta & -\rho(1-\cos\theta) & 0 & 0 & 1 & -\rho(\theta-\sin\theta) \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x \\ x' \\ y \\ y' \\ z \\ \delta \end{pmatrix}_{1}$$
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## **Matrix Example: Strong Focusing**

Consider a doublet of thin quadrupoles separated by drift L

L

 $f_F$ 

Thin quadrupole matrices

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$$M_{\text{doublet}} = \begin{pmatrix} 1 & 0\\ \frac{1}{f_D} & 1 \end{pmatrix} \begin{pmatrix} 1 & L\\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0\\ -\frac{1}{f_F} & 1 \end{pmatrix} = \begin{pmatrix} 1 - \frac{L}{f_F} & L\\ \frac{1}{f_D} - \frac{1}{f_F} - \frac{L}{f_F f_D} & 1 + \frac{L}{f_D} \end{pmatrix}$$

$$f_F, f_D > 0 \qquad \qquad \frac{1}{f_{\text{doublet}}} = \frac{1}{f_D} - \frac{1}{f_F} - \frac{L}{f_F f_D} \qquad (\text{C\&M 5.1 with } f_F = -f_D)$$

$$f_D = f_F = f \quad \Rightarrow \quad \frac{1}{f_{\text{doublet}}} = -\frac{L}{f^2}$$

There is **net focusing** given by this **alternating gradient** system A fundamental point of optics, and of accelerator **strong focusing** 



#### **Strong Focusing: Another View**



$$M_{\text{doublet}} = \begin{pmatrix} 1 & 0\\ \frac{1}{f_D} & 1 \end{pmatrix} \begin{pmatrix} 1 & L\\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0\\ -\frac{1}{f_F} & 1 \end{pmatrix} = \begin{pmatrix} 1 - \frac{L}{f_F} & L\\ \frac{1}{f_D} - \frac{1}{f_F} - \frac{L}{f_F f_D} & 1 + \frac{L}{f_D} \end{pmatrix}$$

incoming paraxial ray 
$$\begin{pmatrix} x \\ x' \end{pmatrix} = M_{\text{doublet}} \begin{pmatrix} x_0 \\ 0 \end{pmatrix} = \begin{pmatrix} 1 - \frac{L}{f_F} \\ \frac{1}{f_D} - \frac{1}{f_F} - \frac{L}{f_F f_D} \end{pmatrix} x_0$$

For this to be focusing, x' must have opposite sign of x where these are coordinates of transformation of incoming paraxial ray

$$f_F = f_D$$
  $x' < 0$  **BUT**  $x > 0$  iff  $f_F > L$ 

Equal strength doublet is net focusing under condition that each lens' focal length is greater than distance between them

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# **Transport Matrix Stability Criteria**

- For long systems (rings) we want  $M^n \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$  stable as  $n \to \infty$ 
  - If 2x2 M has eigenvectors  $(V_1, V_2)$  and eigenvalues  $(\lambda_1, \lambda_2)$ :  $M^n \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix} = A\lambda_1^n V_1 + B\lambda_2^n V_2$
  - M is also unimodular (det M=1) so  $\lambda_{1,2} = e^{\pm i\mu}$  with complex  $\mu$
  - For  $\lambda_{1,2}^n$  to remain bounded,  $\mu$  must be real
  - We can always transform M into diagonal form with the eigenvalues on the diagonal (since det M=1); this does not change the trace of the matrix

$$e^{i\mu} + e^{-i\mu} = 2\cos\mu = \operatorname{Tr} M$$

• The **stability requirement** for these types of matrices is then

 $\mu \text{ real } \Rightarrow -$ 

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$$-1 \le \frac{1}{2} \operatorname{Tr} M \le 1$$



### More Math: Hill's Equation

• Let's go back to our quadrupole equations of motion for  $R \to \infty$ x'' + Kx = 0 y'' - Ky = 0  $K \equiv \frac{1}{(B\rho)} \left(\frac{\partial B_y}{\partial x}\right)$ 

What happens when we let the focusing K vary with s? Also assume K is **periodic** in s with some periodicity C

$$x'' + K(s)x = 0$$
  $K(s) \equiv \frac{1}{(B\rho)} \left(\frac{\partial B_y}{\partial x}\right)(s)$   $K(s+C) = K(s)$ 

This periodicity can be one revolution around the accelerator or as small as one repeated "cell" of the layout

The simple harmonic oscillator equation with a **periodically** varying spring constant K(s) is known as **Hill's Equation** 



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# **Hill's Equation Solution Ansatz**

$$x'' + K(s)x = 0$$
  $K \equiv \frac{1}{(B\rho)} \left(\frac{\partial B_y}{\partial x}\right)(s)$ 

Solution is a quasi-periodic harmonic oscillator

$$x(s) = A w(s) \cos[\Psi(s) + \Psi_0]$$

where w(s) is periodic in C but the phase  $\Psi(s)$  is not!! Substitute this educated guess ("ansatz") to find  $x' = Aw' \cos[\Psi + \Psi_0] - Aw\Psi' \sin[\Psi + \Psi_0]$   $x'' = A(w'' - w\Psi'^2) \cos[\Psi + \Psi_0] - A(2w'\Psi' + w\Psi'') \sin[\Psi + \Psi_0]$  $x'' + K(s)x = -A(2w'\Psi' + w\Psi'') \sin(\Psi + \Psi_0) + A(w'' - w\Psi'^2 + Kw) \cos(\Psi + \Psi_0) = 0$ 

For w(s) and  $\Psi(s)$  to be independent of  $\Psi_0$ , coefficients of the sin and cos terms must vanish identically

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#### **Courant-Snyder Parameters**

$$2ww'\Psi' + w^2\Psi'' = (w^2\Psi')' = 0 \quad \Rightarrow \quad \Psi' = \frac{k}{w(s)^2}$$

$$w'' - (k^2/w^3) + Kw = 0 \implies w^3(w'' + Kw) = k^2$$

Notice that in both equations  $w^2 \propto k$  so we can scale this out and define a new set of functions, **Courant-Snyder Parameters or Twiss Parameters** 

$$\beta(s) \equiv \frac{w^2(s)}{k} \qquad \qquad \Psi' = \frac{1}{\beta(s)} \qquad \Psi(s) = \int \frac{ds}{\beta(s)}$$

$$\alpha(s) \equiv -\frac{1}{2}\beta'(s) \qquad \Rightarrow \qquad K\beta = \gamma + \alpha'$$

$$\gamma(s) \equiv \frac{1 + \alpha(s)^2}{\beta(s)} \qquad \Rightarrow \beta(s), \alpha(s), \gamma(s) \text{ are all periodic in } C$$

$$\Psi(s) \text{ is not periodic in } C$$

$$\Psi(s) \text{ is not periodic in } C$$

### **Towards The Matrix Solution**

What is the matrix for this Hill's Equation solution?

$$x(s) = A\sqrt{\beta(s)} \cos \Psi(s) + B\sqrt{\beta(s)} \sin \Psi(s)$$
  
Take a derivative with respect to s to get  $x' \equiv \frac{dx}{ds}$   
$$\Psi' = \frac{1}{\beta(s)} \quad x'(s) = \frac{1}{\sqrt{\beta(s)}} \{ [B - \alpha(s)A] \cos \Psi(s) - [A + \alpha(s)B] \sin \Psi(s) \}$$

Now we can solve for A and B in terms of initial conditions 
$$(x(0), x'(0))$$
  
 $x_0 \equiv x(0) = A\sqrt{\beta(0)}$   $x'_0 \equiv x'(0) = \frac{1}{\sqrt{\beta(0)}} [B - \alpha(0)A]$   
 $A = \frac{x_0}{\sqrt{\beta(0)}}$   $B = \frac{1}{\sqrt{\beta(0)}} [\beta(0)x'_0 + \alpha(0)x_0]$ 

And take advantage of the periodicity of  $\beta$ ,  $\alpha$  to find x(C), x'(C)

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Hill's Equation Matrix Solution  

$$x(s) = A\sqrt{\beta(s)} \cos \Psi(s) + B\sqrt{\beta(s)} \sin \Psi(s)$$

$$x'(s) = \frac{1}{\sqrt{\beta(s)}} \{ [B - \alpha(s)A] \cos \Psi(s) - [A + \alpha(s)B] \sin \Psi(s) \}$$

$$A = \frac{x_0}{\sqrt{\beta(0)}} \quad B = \frac{1}{\sqrt{\beta(0)}} [\beta(0)x'_0 + \alpha(0)x_0]$$

$$x(C) = [\cos \Psi(C) + \alpha(0) \sin \Psi(C)] x_0 + \beta(0) \sin \Psi(C) x'_0$$
  
$$x'(C) = -\gamma(0) \sin \Psi(C) x_0 + [\cos \Psi(C) - \alpha(0) \sin \Psi(C)] x'_0$$

We can write this down in a matrix form where  $\mu = \Psi(C) - \Psi(0)$  is the betatron phase advance through one period C

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s_0+C} = \begin{pmatrix} \cos \mu + \alpha(0) \sin \mu & \beta(0) \sin \mu \\ -\gamma(0) \sin \mu & \cos \mu - \alpha(0) \sin \mu \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0}$$
$$\mu = \int_{s_0}^{s_0+C} \frac{ds}{\beta(s)} \quad \text{phase advance per cell}$$
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# **Interesting Observations**



- µ is independent of s: this is the betatron phase
   advance of this periodic system
- Determinant of matrix M is still 1!
- Looks like a rotation and some scaling
- M can be written down in a beautiful and deep way

$$M = I \cos \mu + J \sin \mu \quad I = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} \quad J(s_0) \equiv \begin{pmatrix} \alpha(0) & \beta(0) \\ -\gamma(0) & -\alpha(0) \end{pmatrix}$$
$$\boxed{J^2 = -I \quad \Rightarrow \quad M = e^{J(s)\mu}}$$
remember  
$$x(s) = A\sqrt{\beta(s)} \cos[\Psi(s) + \Psi_0]$$
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## **Convenient Calculations**

 If we know the transport matrix M, we can find the lattice parameters (periodic in C)

 $\begin{pmatrix} x \\ x' \end{pmatrix}_{s_0+C} = \begin{pmatrix} \cos\mu + \alpha(0)\sin\mu & \beta(0)\sin\mu \\ -\gamma(0)\sin\mu & \cos\mu - \alpha(0)\sin\mu \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}_{\alpha}$ betatron phase advance per cell  $\cos \mu = \frac{1}{2} \operatorname{Tr} M$  $\beta(0) = \beta(C) = \frac{m_{12}}{\sin \mu}$  $\alpha(0) = \alpha(C) = \frac{m_{11} - \cos \mu}{\sin \mu}$  $\gamma(0) \equiv \frac{1 + \alpha^2(0)}{\beta(0)}$ 

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#### **General Non-Periodic Transport Matrix**

• We can parameterize a general non-periodic transport matrix from s<sub>1</sub> to s<sub>2</sub> using lattice parameters and  $\Delta \Psi = \Psi(s_2) - \Psi(s_1)$ 

$$M_{s_1 \to s_2} = \begin{pmatrix} \sqrt{\frac{\beta(s_2)}{\beta(s_1)}} [\cos \Delta \Psi + \alpha(s_1) \sin \Delta \Psi] & \sqrt{\beta(s_1)\beta(s_2)} \sin \Delta \Psi \\ -\frac{[\alpha(s_2) - \alpha(s_1)] \cos \Delta \Psi + [1 + \alpha(s_1)\alpha(s_2)] \sin \Delta \Psi}{\sqrt{\beta(s_1)\beta(s_2)}} & \sqrt{\frac{\beta(s_1)}{\beta(s_2)}} [\cos \Delta \Psi - \alpha(s_2) \sin \Delta \Psi] \end{pmatrix}$$
(C&M Eqn 5.52)

• This does not have a pretty form like the periodic matrix However both can be expressed as  $M = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix}$ 

where the C and S terms are cosine-like and sine-like; the second row is the s-derivative of the first row! A common use of this matrix is the  $m_{12}$  term:

$$\Delta x(s_2) = \sqrt{\beta(s_1)\beta(s_2)} \sin(\Delta \Psi) x'(s_1)$$

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Effect of angle kick on downstream position



#### (Deriving the Non-Periodic Transport Matrix)

$$x(s) = Aw(s)\cos\Psi(s) + Bw(s)\sin\Psi(s)$$

$$x'(s) = A\left(w'(s)\cos\Psi(s) - \frac{\sin\Psi(s)}{w(s)}\right) + B\left(w'(s)\sin\Psi(s) + \frac{\cos\Psi(s)}{w(s)}\right)$$

Calculate A, B in terms of initial conditions  $(x_0, x'_0)$  and  $(w_0, \Psi_0)$ 

$$A = \left(w_0' \sin \Psi_0 + \frac{\cos \Psi_0}{w_0}\right) x_0 - (w_0 \sin \Psi_0) x_0'$$
$$B = -\left(w_0' \cos \Psi_0 - \frac{\sin \Psi_0}{w_0}\right) x_0 + (w_0 \cos \Psi_0) x_0'$$

Substitute (A,B) and put into matrix form:  $\begin{pmatrix} x(s) \\ x'(s) \end{pmatrix} = \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$ 

$$m_{11}(s) = \frac{w(s)}{w_0} \cos \Delta \Psi - w(s)w'_0 \sin \Delta \Psi \qquad \Delta \Psi \equiv \Psi(s) - \Psi_0$$
$$m_{12}(s) = w(s)w_0 \sin \Delta \Psi \qquad w(s) = \sqrt{\beta(s)}$$

$$m_{21}(s) = -\frac{1 + w(s)w_0w'(s)w'_0}{w(s)w_0}\sin\Delta\Psi - \left[\frac{w'_0}{w(s)} - \frac{w'(s)}{w_0}\right]\cos\Delta\Psi$$

$$m_{22}(s) = \frac{w_0}{w(s)} \cos \Delta \Psi + w_0 w' \sin \Delta \Psi$$

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# **Non-Periodic Transport Matrix**

• C-M 5.52, a very general form from all that math:

$$M(s) = \begin{pmatrix} \sqrt{\frac{\beta(s)}{\beta_0}} [\cos \mu(s) + \alpha_0 \sin \mu(s)] & \sqrt{\beta_0 \beta(s)} \sin \mu(s) \\ -\frac{[\alpha(s) - \alpha_0] \cos \mu(s) + [1 + \alpha_0 \alpha(s)] \sin \mu(s)}{\sqrt{\beta_0 \beta(s)}} & \sqrt{\frac{\beta_0}{\beta(s)}} [\cos \mu(s) - \alpha(s) \sin \mu(s)] \end{pmatrix}$$

- This is how one can parameterize uncoupled x or y transport from one location s<sub>0</sub> to another location s where the Twiss parameters of those locations and their relative phase advance is known
  - Such as from a table from a modeling code like madx
- Most modeling codes can also output matrix elements between specific locations at starts or ends of magnets
  - This still follows the (C S ; C' S') matrix form!

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#### Review

Hill's equation x'' + K(s)x = 0quasi – periodic ansatz solution  $x(s) = A\sqrt{\beta(s)}\cos[\Psi(s) + \Psi_0]$ 

$$\beta(s) = \beta(s+C) \quad \gamma(s) \equiv \frac{1+\alpha(s)^2}{\beta(s)}$$
$$\alpha(s) \equiv -\frac{1}{2}\beta'(s) \quad \Psi(s) = \int \frac{ds}{\beta(s)}$$

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s_0+C} = \begin{pmatrix} \cos \mu + \alpha(0) \sin \mu & \beta(0) \sin \mu \\ -\gamma(0) \sin \mu & \cos \mu - \alpha(0) \sin \mu \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0}$$

betatron phase advance

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$$\mu = \int_{s_0}^{s_0 + C} \frac{ds}{\beta(s)}$$

$$\operatorname{Tr} M = 2\cos\mu$$

$$M = I\cos\mu + J\sin\mu \quad I = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} \quad J(s_0) \equiv \begin{pmatrix} \alpha(0) & \beta(0) \\ -\gamma(0) & -\alpha(0) \end{pmatrix}$$

$$J^2 = -I \Rightarrow M = e^{J(s)\mu}$$
  
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### (Lunch break)



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- Most accelerator lattices are designed in modular ways
  - Design and operational clarity, separation of functions
- One of the most common modules is a FODO module
  - Alternating focusing and defocusing "strong" quadrupoles
  - Spaces between are combinations of drifts and dipoles
  - Strong quadrupoles dominate the focusing

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- Periodicity is one FODO "cell" so we'll investigate that motion
- Horizontal beam size largest at centers of focusing quads
- Vertical beam size largest at centers of defocusing quads





- Select periodicity between centers of focusing quads
  - A natural periodicity if we want to calculate maximum β(s)

$$M = \begin{pmatrix} 1 & 0 \\ -\frac{1}{2f} & 1 \end{pmatrix} \begin{pmatrix} 1 & \frac{L}{2} \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ \frac{1}{f} & 1 \end{pmatrix} \begin{pmatrix} 1 & \frac{L}{2} \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ -\frac{1}{2f} & 1 \end{pmatrix}$$
$$M = \begin{pmatrix} 1 - \frac{L^2}{8f^2} & \frac{L^2}{4f} + L \\ \frac{L^2}{16f^3} - \frac{L}{4f^2} & 1 - \frac{L^2}{8f^2} \end{pmatrix} \qquad \text{Tr} M = 2\cos\mu = 2 - \frac{L^2}{4f^2}$$

$$1 - \frac{L^2}{8f^2} = \cos\mu = 1 - 2\sin^2\frac{\mu}{2} \implies \sin\frac{\mu}{2} = \pm\frac{L}{4f}$$

•  $\mu$  only has real solutions (stability) if  $\frac{L}{4} < f$ 



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• What is the maximum beta function,  $\hat{\beta}$  ?

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A natural periodicity if we want to calculate maximum β(s)

$$M = \begin{pmatrix} 1 - \frac{L^2}{8f^2} & \frac{L^2}{4f} + L \\ \frac{L^2}{16f^3} - \frac{L}{4f^2} & 1 - \frac{L^2}{8f^2} \end{pmatrix} \Leftrightarrow m_{12} = \beta \sin \mu$$
$$\hat{\beta} \sin \mu = \frac{L^2}{4f} + L = L\left(1 + \sin\frac{\mu}{2}\right) \qquad \qquad \hat{\beta} = \frac{L}{\sin\mu}\left(1 + \sin\frac{\mu}{2}\right)$$

 Follow a similar strategy reversing F/D quadrupoles to find the minimum β(s) within a FODO cell (center of D quad)

$$\check{\beta} = \frac{L}{\sin\mu} \left( 1 - \sin\frac{\mu}{2} \right)$$







- This is a picture of a FODO lattice, showing contours of  $\pm \sqrt{\beta(s)}$  since the particle motion goes like  $x(s) = A\sqrt{\beta(s)} \cos[\Psi(s) + \Psi_0]$ 
  - This also shows a particle oscillating through the lattice
  - Note that  $\sqrt{\beta(s)}$  provides an "envelope" for particle oscillations
    - $\sqrt{\beta(s)}$  is sometimes called the envelope function for the lattice
  - Min beta is at defocusing quads, max beta is at focusing quads
  - 6.5 periodic FODO cells per betatron oscillation

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 $\Rightarrow \quad \mu = 360^{\circ}/6.5 \approx 55^{\circ}$ 





- 1/6 of one of two RHIC synchrotron rings, injection lattice
  - FODO cell length is about L=30 m
  - Phase advance per FODO cell is about  $\mu = 77^{\circ} = 1.344$  rad

$$\hat{\beta} = \frac{L}{\sin \mu} \left( 1 + \sin \frac{\mu}{2} \right) \approx 53 \text{ m}$$
$$\check{\beta} = \frac{L}{\sin \mu} \left( 1 - \sin \frac{\mu}{2} \right) \approx 8.7 \text{ m}$$

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## **Propagating Lattice Parameters**

• If I have  $(\beta, \alpha, \gamma)(s_1)$  and I have the transport matrix  $M(s_1, s_2)$ that transports particles from  $s_1 \rightarrow s_2$ , how do I find the new lattice parameters  $(\beta, \alpha, \gamma)(s_2)$ ?

$$M(s_1, s_1 + C) = I \cos \mu + J \sin \mu = \begin{pmatrix} \cos \mu + \alpha(s_1) \sin \mu & \beta(s_1) \sin \mu \\ -\gamma(s_1) \sin \mu & \cos \mu - \alpha(s_1) \sin \mu \end{pmatrix} = \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix}$$

#### Homework 🙂





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## **Propagating Lattice Parameters**

• If I have  $(\beta, \alpha, \gamma)(s_1)$  and I have the transport matrix  $M(s_1, s_2)$ that transports particles from  $s_1 \rightarrow s_2$ , how do I find the new lattice parameters  $(\beta, \alpha, \gamma)(s_2)$ ?

$$M(s_{1}, s_{1} + C) = I \cos \mu + J \sin \mu = \begin{pmatrix} \cos \mu + \alpha(s_{1}) \sin \mu & \beta(s_{1}) \sin \mu \\ -\gamma(s_{1}) \sin \mu & \cos \mu - \alpha(s_{1}) \sin \mu \end{pmatrix} = \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix}$$
  
The J(s) matrices at s<sub>1</sub>, s<sub>2</sub> are related by  
$$J(s_{2}) = M(s_{1}, s_{2})J(s_{1})M^{-1}(s_{1}, s_{2})$$
  
Then expand, using det M=1  
Your homework is to then show...

$$\begin{pmatrix} \beta(s_2) \\ \alpha(s_2) \\ \gamma(s_2) \end{pmatrix} = \begin{pmatrix} m_{11}^2 & -2m_{11}m_{12} & m_{12}^2 \\ -m_{11}m_{21} & m_{11}m_{22} + m_{12}m_{21} & -m_{12}m_{22} \\ m_{21}^2 & -2m_{21}m_{22} & m_{22}^2 \end{pmatrix} \begin{pmatrix} \beta(s_1) \\ \alpha(s_1) \\ \gamma(s_1) \end{pmatrix}$$

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beam particles in phase space is related to the emittance

We can express this in terms of our lattice functions!

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#### **Invariants and Ellipses**

$$x(s) = A\sqrt{\beta(s)}\cos[\phi(s) + \phi_0]$$

We assumed A was constant, an invariant of the motion

A can be expressed in terms of initial coordinates to find

 $\mathcal{W} \equiv A^2 = \gamma_0 x_0^2 + 2\alpha_0 x_0 x_0' + \beta_0 x_0'^2$ 

This is known as the **Courant-Snyder invariant**: for all s,  $\mathcal{W} = \gamma(s)x(s)^2 + 2\alpha(s)x(s)x'(s) + \beta(s)x'(s)^2$ 

Similar to total energy of a simple harmonic oscillator

 ${\mathcal W}$  looks like an elliptical area in (x,x') phase space

Our matrices look like scaled rotations (ellipses) in phase space



# Emittance

The area of the ellipse inscribed by any given particle in phase space as it travels through our accelerator is called the **emittance** *i*: it is "constant" and given by

 $\epsilon = \pi \mathcal{W} = \pi [\gamma(s)x(s)^2 + 2\alpha(s)x(s)x'(s) + \beta(s)x'(s)^2]$ 

Emittance is often quoted as the area of the ellipse that would contain a certain fraction of all (Gaussian) beam particles e.g. RMS emittance contains 39% of 2D beam particles Related to RMS beam size  $\sigma_{RMS}$  $\sigma_{RMS} = \sqrt{\epsilon\beta(s)}$ RMS beam size depends on s! RMS emittance convention is fairly standard for electron rings, with units of mm-mrad

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### **Adiabatic Damping and Normalized Emittance**

- But we introduce electric fields when we accelerate
  - When we accelerate, invariant emittance is not invariant!
  - We are defining areas in (x, x') phase space
  - The definition of x doesn't change as we accelerate
  - But  $x' \equiv dx/ds = p_x/p_0$  does since  $p_0$  changes!
  - $p_0$  scales with relativistic beta, gamma:  $p_0 \propto eta \gamma$
  - This has the effect of compressing x' phase space by  $\beta\gamma$



 Normalized emittance is the invariant in this case *e*<sub>N</sub> = unnormalized emittance goes down as we accelerate
 This is called adiabatic damping, important in, e.g., linacs

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 Now we can figure out some things from a phase space ellipse at a given s coordinate:

> $x_1 = \sqrt{\mathcal{W}/\gamma(s)}$   $x_2 = \sqrt{\mathcal{W}\beta(s)}$  $y_1 = \sqrt{\mathcal{W}/\beta(s)}$   $y_2 = \sqrt{\mathcal{W}\gamma(s)}$

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#### **Rings and Tunes**

- A synchrotron is by definition a periodic focusing system
  - It is very likely made up of many smaller periodic regions too
  - We can write down a periodic **one-turn matrix** as before

$$M = I\cos\mu + J\sin\mu \quad I = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} \quad J(s_0) \equiv \begin{pmatrix} \alpha(0) & \beta(0) \\ -\gamma(0) & -\alpha(0) \end{pmatrix}$$

- We define **tune** as the total betatron phase advance in one revolution around a ring divided by the total angle  $2\pi$ 

$$Q_{x,y} = \frac{\Delta \mu_{x,y}}{\Delta \theta} = \frac{1}{2\pi} \oint \frac{ds}{\beta_{x,y}(s)}$$

a) Horizontal Betatron Oscillation with tune: Q<sub>h</sub> = 6.3, i.e., 6.3 oscillations per turn. T. Satogata / January 2017 b) Vertical Betatron Oscillation with tune: Q<sub>v</sub> = 7.5, i.e., 7.5 oscillations per turn. USPAS Accelerator Physics



# Tunes

- There are horizontal and vertical tunes
  - turn by turn oscillation frequency

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- Tunes are a direct indication of the amount of focusing in an accelerator
  - Higher tune implies tighter focusing, lower  $\langle \beta_{x,y}(s) \rangle$
- Tunes are a critical parameter for accelerator performance
  - Linear stability depends greatly on phase advance
  - Resonant instabilities can occur when  $nQ_x + mQ_y = k$
  - Often adjusted by changing groups of quadrupoles

 $M_{\text{one turn}} = I\cos(2\pi Q) + J\sin(2\pi Q)$ 



# 6.2: Stability Diagrams

- Designers often want or need to change the focusing of the two transverse planes in a FODO structure
  - What happens if the focusing/defocusing strengths differ?



• Recalculate the M matrix and use dimensionless quantities  $F \equiv \frac{L}{2f_F}$   $D \equiv \frac{L}{2f_D}$ 

then take the trace for stability conditions to find

$$\cos \mu = 1 + D - F - \frac{FD}{2}$$
  $\sin^2 \frac{\mu}{2} = \frac{FD}{4} + \frac{F - L}{2}$ 

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# **Stability Diagrams II**

$$\cos \mu = 1 + D - F - \frac{FD}{2}$$
  $\sin^2 \frac{\mu}{2} = \frac{FD}{4} + \frac{F - D}{2}$ 

- For stability, we must have  $-1 < \cos \mu < 1$
- Using  $\cos \mu = 1 2\sin^2 \frac{\mu}{2}$ , stability limits are where  $\sin^2 \frac{\mu}{2} = 0$   $\sin^2 \frac{\mu}{2} = 1$
- These translate to a FODO "necktie" stability diagram



Figure. 6.1 Stability or "necktie" diagram for an alternate focusing lattice. The shaded area is the region of stability.

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**Onwards to the computer lab...** 

# Introduction to MAD-X

#### G. Sterbini, CERN Thanks to W. Herr and B. Holzer

14 January 2014, Archamps And T. Satogata at USPAS 2017

http://indico.cern.ch/event/286275/contributions/651708/attachments/531417/732835/juas.pdf

http://toddsatogata.net/2017-USPAS/lab/lab1.pdf



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